Drake Street

Traffic Impact Analysis

Columbia, South Carolina

November 2022



Prepared for:

Terra Alta Ventures



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1 INTRODUCTION

This report presents the Drake Street traffic impact analysis (TIA) findings. The proposed development will be located off Drake Street between Norris Street and Clifton Street in Columbia, SC (see **Figure 1-1**). The proposed development will consist of 150 multi-family residential units and will be constructed by 2023.

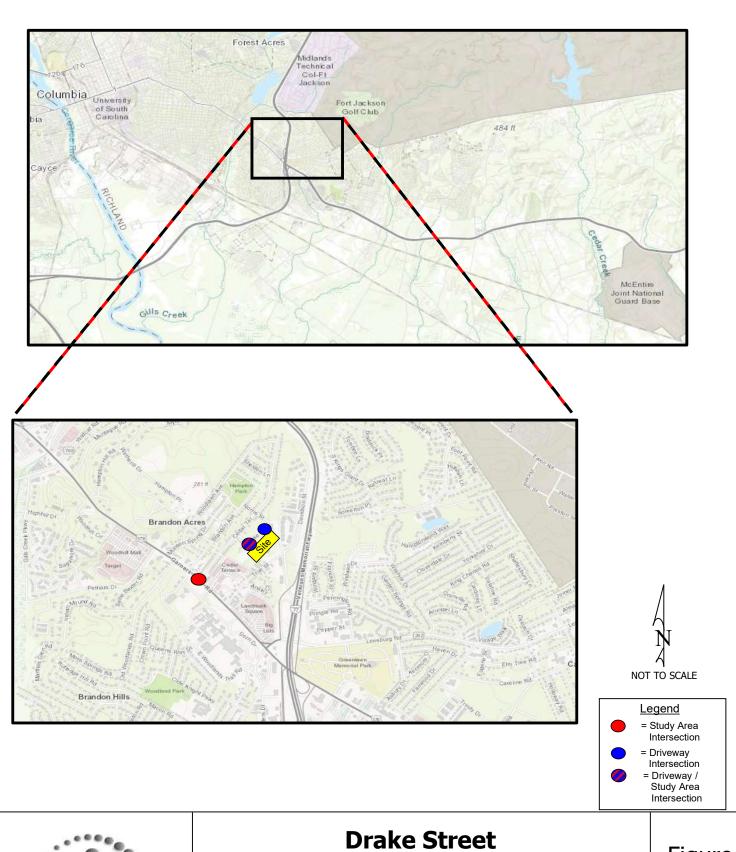
Analyses were completed for the following scenarios:

- 2022 Existing traffic volumes;
- 2023 Background traffic volumes; and
- 2023 Build traffic volumes (Background + site trips).

The purpose of this TIA is to verify that the existing geometry provided within the study area is sufficient to accommodate the projected traffic volumes, and to determine what, if any, improvements are necessary.

The following steps were taken to determine the potential traffic impacts associated with this project:

- 1. <u>Data Collection</u> AM (7:00 9:00) and PM (4:00 6:00) peak period turning movement counts were collected in August 2022 at the following intersections:
 - US-76 (Garners Ferry Road) / Cedar Terrace unsignalized; and
 - Drake Street / Clifton Street unsignalized.
- 2. <u>Trip Generation/Future Traffic</u> Traffic generated by the proposed development was estimated using the 11th Edition of the Institute of Transportation Engineers <u>Trip Generation Manual</u>. Trip generation was calculated for the development following SCDOT standards and practices for trip generation. Projected traffic volumes were calculated using a 2% ambient growth rate. Per discussion with City staff, there are currently two (2) approved developments within the project study area.
- 3. <u>Trip Distribution and Projections</u> The site-generated trip distribution was based on existing area traffic and engineering judgement. It was assumed, for purposes of analysis, that projected trips for the Drake Street Development would follow similar patterns as existing traffic.
- 4. <u>Traffic Capacity Analysis</u> Level of service analyses were performed using Synchro Version 10.3 for the following intersections:
 - Garners Ferry Road / Cedar Terrace;
 - Drake Street / Clifton Street / Site Access 1; and
 - Drake Street / Site Access 2.





Drake Street
Traffic Impact Analysis
Site Location Map

Figure 1-1

2 EXISTING INFORMATION

The proposed development will be located off Drake Street between Norris Street and Clifton Street in Columbia, SC (see **Figure 1-1**).

2.1 STUDY LIMITS

Access to the proposed site will be provided via two (2) full movement connections to Drake Street. Site accesses are shown graphically in **Figure 1-1** and the preliminary site layout in **Figure 2-1**. All figures are located at the end of their respective chapter.

The study limits include the following three (3) intersections:

- Garners Ferry Road / Cedar Terrace;
- Drake Street / Clifton Street / Site Access 1; and
- Drake Street / Site Access 2.

2.2 EXISTING ROADWAYS

US-76 (Garners Ferry Road) is an undivided facility with a varying cross-section, running approximately east-west in the study area. The facility is classified by SCDOT as a principal arterial. Within the study area, US-76 has a posted 40-mph speed limit and provides connection between I-77 and downtown Columbia. Per 2021 SCDOT Average Annual Daily Traffic (AADT) data, US-76 carries 44,300 vehicles per day (VPD) between Rosewood Drive and Leesburg Road.

Cedar Terrace is an undivided facility with a two-lane cross section, running approximately north-south in the study area. Cedar Terrace has a posted 25-mph speed limit and serves residential uses. There is no AADT available for this facility.

Clifton Street is an undivided facility with a two-lane cross section, running approximately east-west in the study area. Clifton Street has a 25-mph speed limit and serves residential uses. There is no AADT available for this facility.

Drake Street is an undivided facility with a two-lane cross section, running approximately north-south in the study area. Drake Street has a 25-mph speed limit and serves residential uses. There is no AADT available for this facility.

2.3 EXISTING INTERSECTIONS

Using available aerial imagery, Timmons Group compiled the existing geometry for each study area intersection. The existing intersection geometry is shown in **Figure 2-2**.

US-76 / Cedar Terrace is an unsignalized intersection with the southbound approach encountering the stop condition. The southbound approach consists of a shared left-turn / right-turn lane. The eastbound approach includes an exclusive left-turn lane and three through lanes. The westbound approach consists of two through lanes and a shared through / right-turn lane.

Drake Street / Clifton Street is an unsignalized intersection with the southbound approach encountering the stop condition. The northbound approach consists of a shared left-turn / through lane. The southbound approach includes a shared through / right-turn lane. The eastbound approach includes a shared left-turn

/ right-turn lane. Due to Synchro limitations this intersection was analyzed as an all-way stop. This represents a worst-case scenario from a delay perspective.

2.4 TRAFFIC VOLUMES

Timmons Group calculated peak hour volumes at the study area intersections using the collected AM (7:00 - 9:00) and PM (4:00 - 6:00) peak period turning movement counts undertaken in August 2022. Collected traffic count data is summarized in **Figure 2-3**. Traffic count data is found in **Appendix B**.

2.5 CAPACITY ANALYSIS

Using aerial photography, and traffic count data, traffic operations were analyzed during 2022 (existing) and 2023 (without and with the proposed development site trips).

Capacity analysis allows traffic engineers to determine the impacts of traffic on the surrounding roadway network. The Transportation Research Board's (TRB) *Highway Capacity Manual* (HCM) methodologies govern how the capacity analyses are conducted and how the results are interpreted. There are six letter grades of Levels of Service (LOS) from A to F, with LOS A representing the best operating conditions and LOS F the worst operating conditions. At signalized intersections, an overall intersection LOS E (or worse) is generally considered unacceptable. Similarly, at unsignalized intersections, a LOS E (or worse) is generally considered unacceptable. Nevertheless, it is not uncommon for side streets to function unacceptably during peak traffic periods because the traffic volumes often do not warrant a traffic signal to assist side street traffic. **Table 2-1** shows in detail how each of these levels of service are interpreted.

Table 2-1: Level of Service Definitions

Level of Service	Roadway Segments or Controlled Access Highways	Intersections	N /
Α	Free flow, low traffic density.	No vehicle waits longer than one signal indication.	
В	Delay is not unreasonable, stable traffic flow.	On a rare occasion motorists wait through more than one signal indication.	
С	Stable condition, movements somewhat restricted due to higher volumes, but not objectionable for motorists.	Intermittently drivers wait through more than one signal indication, and occasionally backups may develop behind left turning vehicles, traffic flow still stable and acceptable.	C
D	Movements more restricted, queues and delays may occur during short peaks, but lower demands occur often enough to permit clearing, thus preventing excessive backups.	Delays at intersections may become extensive with some, especially left-turning vehicles waiting two or more signal indications, but enough cycles with lower demand occur to permit periodic clearance, thus preventing excessive backups.	D
E	Actual capacity of the roadway invloves delay to all motorists due to congestion.	Very long queues may create lengthly delays, especially for left-turning vehicles.	
Е	Forced flow with demand volumes greater than capacity resulting in complete congestion. Volumes drop to zero in extreme cases.	Backups from locations downstream restrict or prevent movement of vehicles out of approach creating a storage ares during part or all of an hour.	F
Streets" - A	A <i>Policy on Design of Design of Urb</i> ASHTO, 1973 based upon materia <i>lanual"</i> , National Academy of Scie	l published in "Highway	

For signalized and unsignalized intersections, level of service is defined in terms of **delay**, a measure of driver discomfort, frustration, fuel consumption and lost travel time. **Table 2-2** summarizes the delay associated with each LOS category:

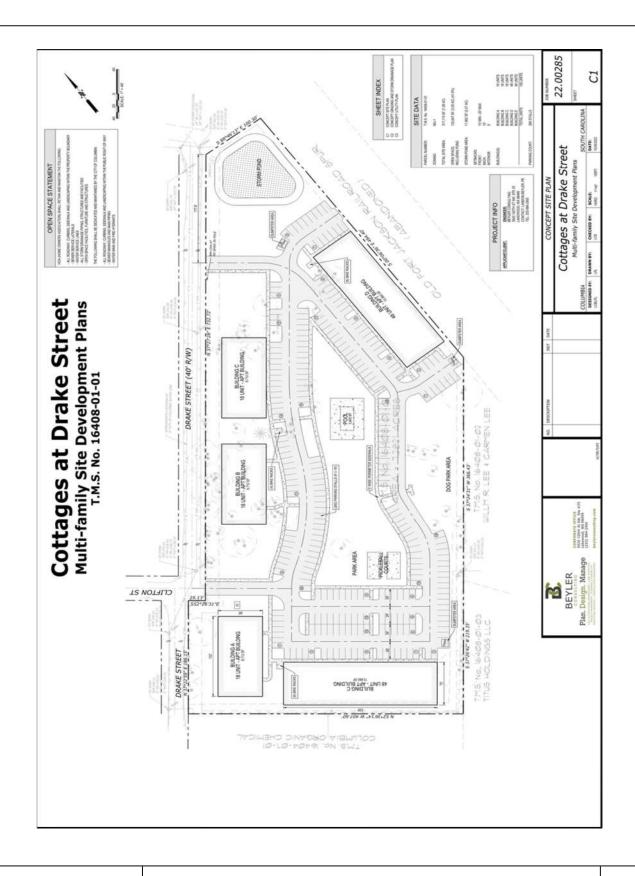
Table 2-2: Signalized and Unsignalized Intersection Level of Service Criteria

Signalize	ed Intersections	Unsignalized Intersections						
Level of Service	Control Delay per Vehicle (sec/veh)	Level of Service	Average Control Delay (sec/veh)					
Α	≤ 10	Α	0 to 10					
В	> 10 to ≤ 20	В	> 10 to ≤ 15					
С	> 20 to ≤ 35	С	> 15 to ≤ 25					
D	> 35 to ≤ 55	D	> 25 to ≤ 35					
Е	> 55 to ≤ 80	Е	> 35 to ≤ 50					
F	> 80	F	> 50					

Source: Exhibit 16-2 and Exhibit 17-2 from TRB's "Highway Capacity Manual 2000"

Capacity analyses were performed to assess operational conditions. Study area intersections were analyzed using Synchro Version 10.3 based on Highway Capacity Manual (HCM) methodologies with the following assumptions:

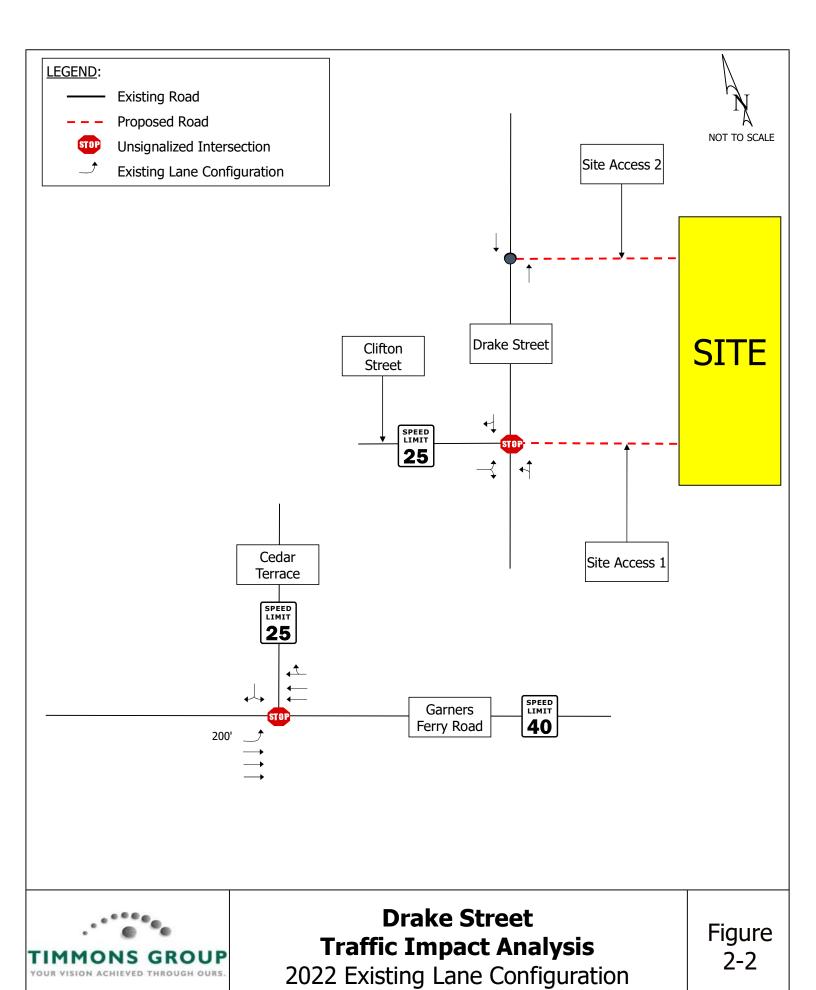
- Existing grades;
- 12-foot lane widths;
- No parking activity, bus stops, or pedestrians;
- Peak hour factor (PHF) of 0.90;
- Heavy vehicle percentages 2%; and
- Minimum turning movement volume of 4 VPH for all allowed movements.

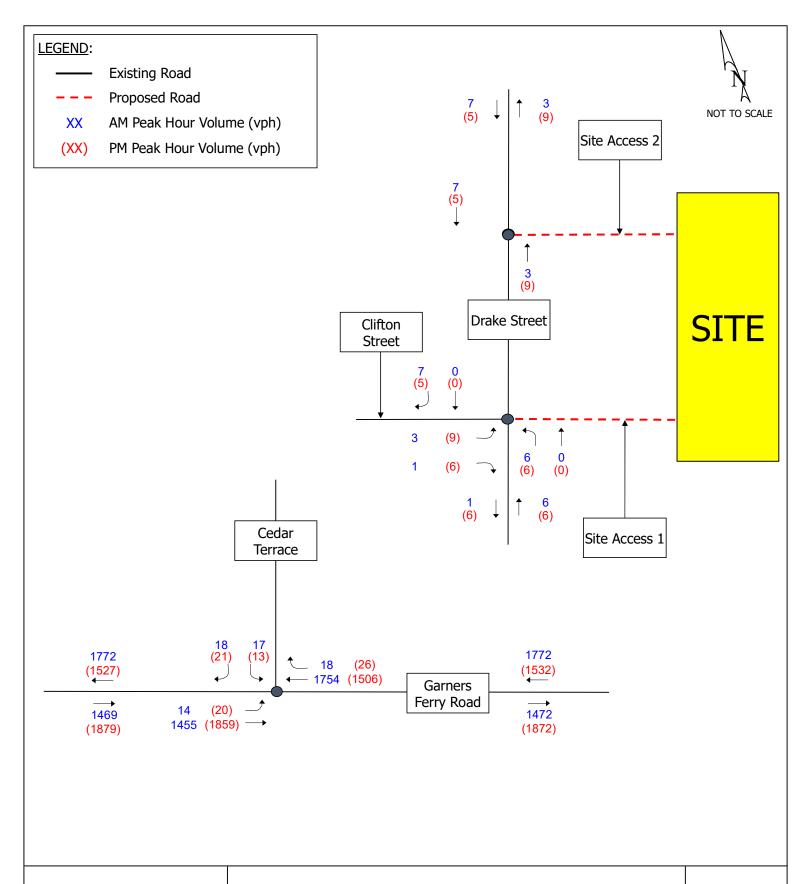




Drake Street Traffic Impact AnalysisPreliminary Site Sketch

Figure 2-1







Drake Street Traffic Impact Analysis2022 Existing Traffic Volumes

Figure 2-3

3 EXISTING AND BACKGROUND CONDITIONS AND ANALYSIS

3.1 2022 EXISTING ANALYSES

Table 3-1 summarizes the 2022 Existing intersection LOS and delay based on the geometry shown in **Figure 2-2** and the 2022 Existing traffic volumes shown in **Figure 2-3**. The corresponding Synchro output is included in **Appendix C**.

The southbound approach of the unsignalized Garners Ferry Road / Cedar Terrace intersection is currently operating at a LOS F during both 2022 Existing peak hours. All other approaches are currently operating at a LOS A during both 2022 Existing peak hours.

All Drake Street / Clifton Street unsignalized intersection approaches are currently operating at a LOS A during both 2022 Existing peak hours.

		AM PEAR	HOUR	PM PEAK HOUR			
Intersection	Movement and Approach	Delay ¹ (sec/veh)	LOS 1	Delay ¹ (sec/veh)	LOS 1		
1: Garners Ferry Road & Ceder Terrace Street	EB Approach	0.3	Α	0.3	Α		
	WB Approach	0.0	Α	0.0	Α		
	SB Approach	125.2	F	79.0	F		
2: Drake Street & Clifton Street	EB Approach	6.8	Α	6.9	Α		
	NB Approach	7.1	Α	7.2	Α		
	SB Approach	6.6	Α	6.7	Α		

Table 3-1: Intersection Level of Service and Delay Summary 2022 Existing Traffic Volumes

3.2 2023 BACKGROUND TRAFFIC VOLUMES

Figure 3-1 shows the 2023 Ambient traffic volumes calculated using a 2% growth rate for one (1) year.

Overall

Per conversations with the City of Columbia, there are two (2) developments assumed to be fully built out by 2023: Murphy Express gas station and the VA Hospital Expansion (see **Appendix D**). Listed below are the approved developments, site trip distribution assumptions, and proposed offsite improvements.

- Murphy Express
 - No TIA provided
 - Located off Garners Ferry Road southeast of the subject development
 - o Gas station (assumed 16 vehicle fueling positions based on site visit).
 - Building gross floor area assumed to be approximately 2,600 SF based on adjacent Murphy Express gas stations

6.8

6.9

A

- Trips calculated using the 11th Edition of the Institute of Transportation Engineers (ITE)
 Trip Generation Manual
- o Land Use Code 945
- Pass-By rates of 76% AM / 75% PM were used per ITE standards
- Based on existing traffic patterns, it is anticipated that approximately 40% of trips generated will traverse the study area (see **Appendix D**)
- No assumed offsite intersection improvements

Overall intersection LOS and delay not reported for TWSC intersections.

VA Expansion

- No TIA provided
- Located off Garners Ferry Road southwest of the subject development
- o 62,500 SF of Medical-Office space
- Trips calculated using the 11th Edition of the Institute of Transportation Engineers (ITE)
 Trip Generation Manual
- o Land Use Code 720
- Based on existing traffic patterns, it is anticipated that approximately 40% of trips generated will traverse the study area (see **Appendix D**)
- No assumed offsite intersection improvements

2023 projected and distributed trips from the approved developments (see **Appendix D**) were totaled and are found in **Figure 3-2**. The 2023 ambient traffic volumes were added to the approved development traffic volumes to calculate the 2023 Background traffic volumes (**Figure 3-3**).

3.3 2023 BACKGROUND ANALYSIS

Table 3-2 summarizes the intersection LOS and delay based on the geometry shown in **Figure 2-2** and the 2023 Background traffic volumes shown in **Figure 3-3**. The corresponding Synchro output is included in **Appendix C**.

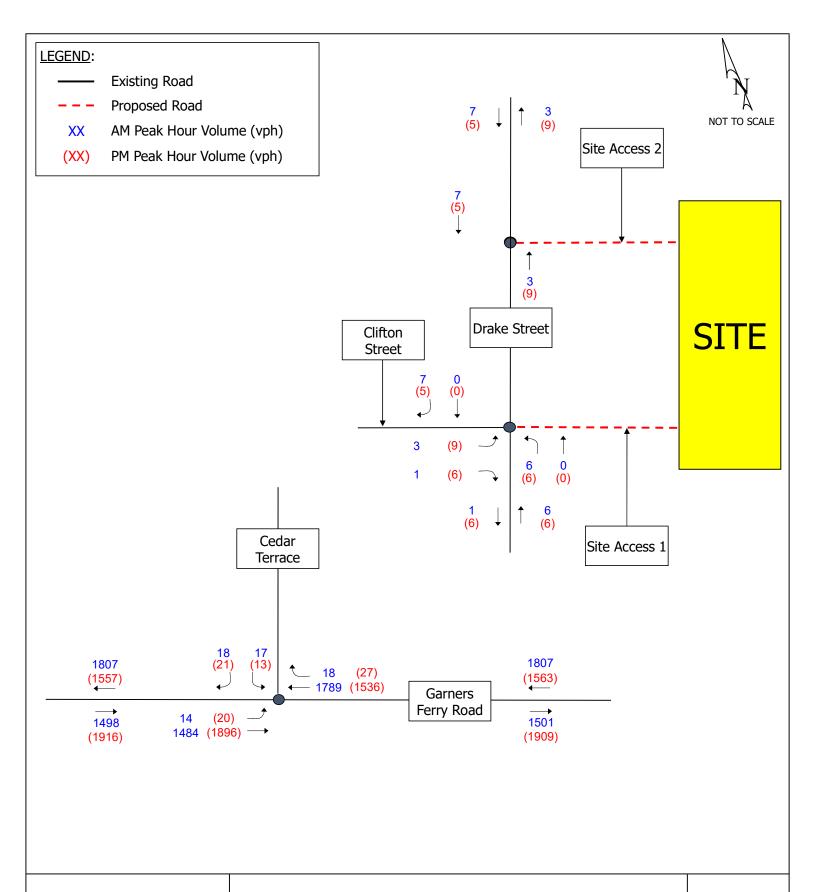
The southbound approach of the unsignalized Garners Ferry Road / Cedar Terrace intersection is projected to operate at a LOS F during both 2023 Background peak hours. All other approaches are projected to operate at a LOS A during both 2023 Background peak hours.

All Drake Street / Clifton Street unsignalized intersection approaches are projected to operate at a LOS A during both 2023 Background peak hours.

Table 3-2: Intersection Level of Service and Delay Summary 2023 Background Traffic Volumes

		AM PEAR	HOUR	PM PEAR	HOUR
Intersection	Movement and Approach	Delay ¹ (sec/veh)	LOS 1	Delay ¹ (sec/veh)	LOS 1
1: Garners Ferry Road & Ceder Terrace Street	EB Approach	0.4	Α	0.3	Α
	WB Approach	0.0	Α	0.0	Α
	SB Approach	163.2	F	102.8	F
2: Drake Street & Clifton Street	EB Approach	6.8	Α	6.9	Α
	NB Approach	7.1	Α	7.2	Α
	SB Approach	6.6	Α	6.7	Α
	Overall	6.8	Α	6.9	Α

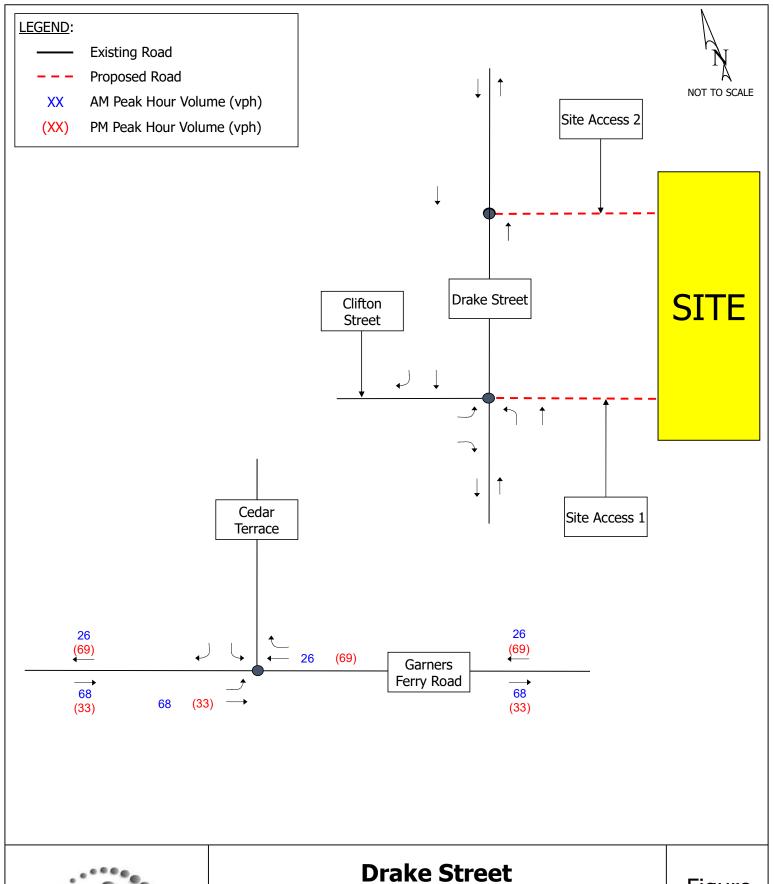
Overall intersection LOS and delay not reported for TWSC intersections.





Drake Street Traffic Impact Analysis2023 Ambient Traffic Volumes

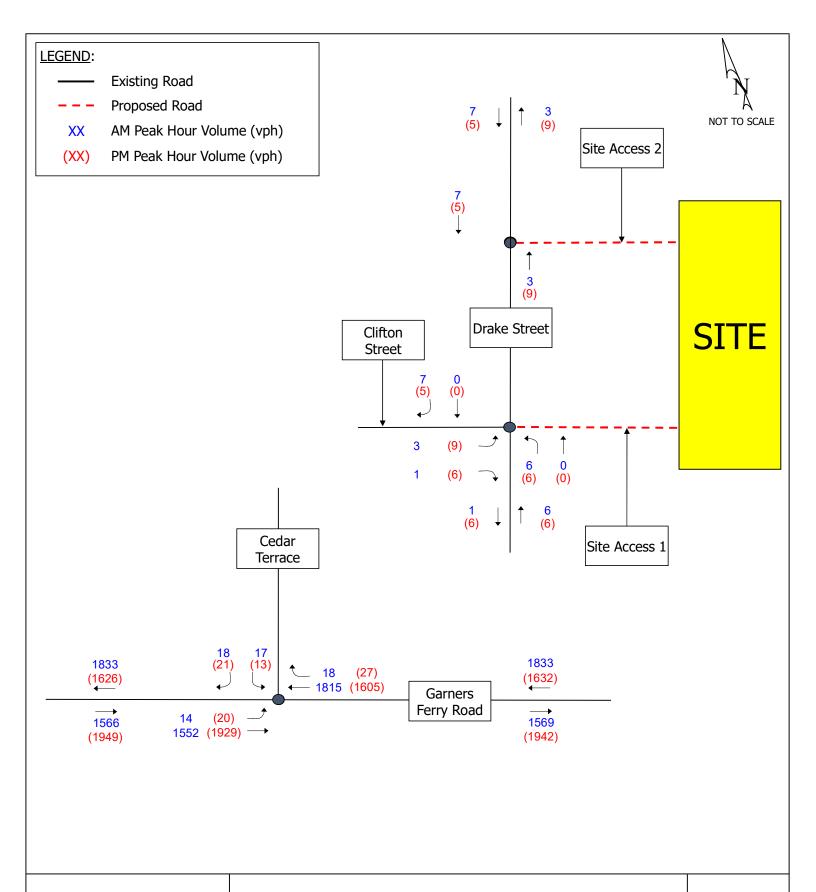
Figure 3-1





Traffic Impact Analysis Approved Development Traffic Volumes

Figure 3-2





Drake Street Traffic Impact Analysis2023 Background Traffic Volumes

Figure 3-3

4 SITE TRIP GENERATION AND DISTRIBUTION

Proposed development site trips were estimated based on the proposed land uses supplied by the developer and subsequently distributed onto the surrounding roadway network.

4.1 TRIP GENERATION

The site-generated trips shown in **Table 4-1** are based on trip generation information provided in the 11th Edition of the Institute of Transportation Engineers (ITE) *Trip Generation Manual* and the anticipated development size. The trip generation was calculated using the proposed number of residential units as the independent variable. The "Peak Hour of Generator" and "Fitted Curve" were used to calculate trips as that combination resulted in the highest number of trips; thus, representing a worst-case scenario from a traffic generation perspective.

Table 4-1: Trip Generation Summary

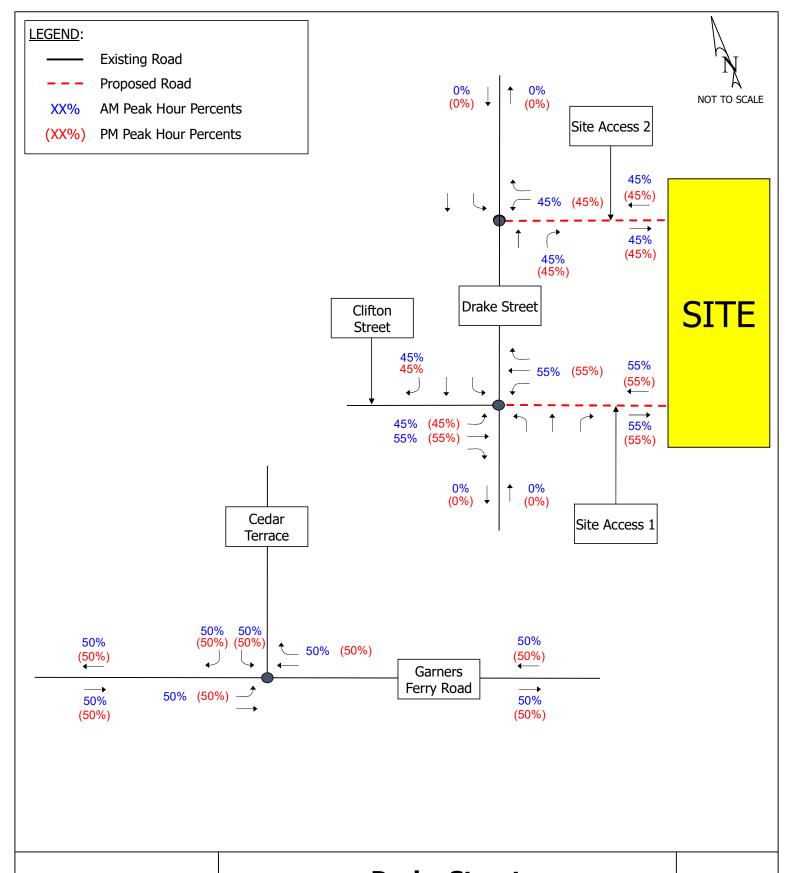
ITE Land Use Code	Independent	ADT	Al	M Peak Ho	our	PM Peak Hour				
TTE Land USE Code	Variable	ADI	In	Out	Total	In	Out	Total		
220- Multifamily Housing (Low-Rise)	150 Units	1,037	19	62	81	61	37	98		

SOURCE: Institute of Transportation Engineers' Trip Generation Manual 11th Edition (2021)

AM peak hour trips totaled 19 incoming and 62 outgoing where PM peak hour trips totaled 61 incoming and 37 outgoing. Average Daily Traffic (ADT) volumes generated by the development totaled 1,037 VPD. No reduction in trips were included due to internal capture or pass-by trips.

4.2 TRIP DISTRIBUTION

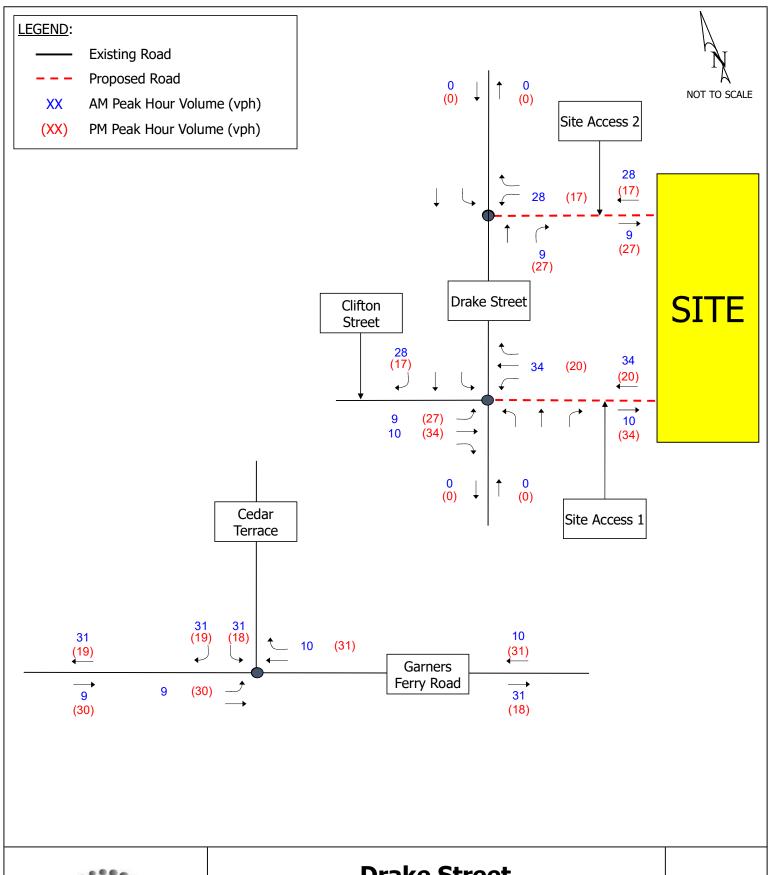
The directional traffic patterns, or trip distribution, of the site-generated traffic was determined using the existing traffic characteristics and engineering judgement. It was assumed, for purposes of this study, that all site traffic would enter and exit the study area in a similar manner as the existing traffic. Area trip distribution is based on traffic counts performed by Timmons Group. Total trips into and out of the study area using Garners Ferry Road form the basis for the percentage distribution. The percentages were routed, via shortest path, to and from the proposed development. The distribution percentages were then applied to the generated trips to predict routes and project traffic volumes for the 2023 Build scenario. Trip distribution percentages are shown in **Figure 4-1** and trip distribution volumes are shown in **Figure 4-2**.





Drake Street Traffic Impact Analysis Trip Distribution Percentages

Figure 4-1





Drake Street Traffic Impact Analysis Trip Distribution Volumes

Figure 4-2

5 2023 BUILD CONDITION AND ANALYSIS

To complete the 2023 Build analyses (including proposed development), the estimated site trips were added to the 2023 Background traffic volumes. The projected total volumes, along with the existing intersection geometry, were used to complete the capacity analyses.

To summarize, the 2023 Build traffic volumes shown in **Figure 5-1** contain the following:

- 2023 Background traffic volumes (Figure 3-3); and
- Site trips generated by the subject development (Figure 4-2).

5.1 2023 BUILD ANALYSIS

Table 5-1 summarizes the intersection LOS and delay based on the geometry shown in **Figure 2-2** and the 2023 Build traffic volumes shown in **Figure 5-1**. The corresponding Synchro output is included in **Appendix C**.

The southbound approach of the unsignalized Garners Ferry Road / Cedar Terrace intersection is projected to operate at a LOS F during both 2023 Build peak hours. All other approaches are projected to operate at a LOS A during both 2023 peak hours. Other than signalization, no amount of feasible geometric improvements will result in the southbound approach operating acceptably. Based on the side street volumes it is unlikely that the subject intersection will meet the MUTCD's 4-hour and 8-hour volume warrants; therefore, signalization is not recommended. Any widening along the southbound approach would likely require obtaining substantial right-of-way and would impact the viability of the adjacent business. Additionally, the widening of Cedar Terrace would likely require the relocation of utilities. Based on aerial imagery, southbound vehicles have several options (i.e. Brandon Avenue and Munsen Spring Drive) to access Garner Ferrys Road should significant delay occur at the Garners Ferry Road / Cedar Terrace intersection. Finally, the adjacent signals will provide gaps in traffic to accommodate southbound vehicles. No improvements are recommended due to the construction of the subject development.

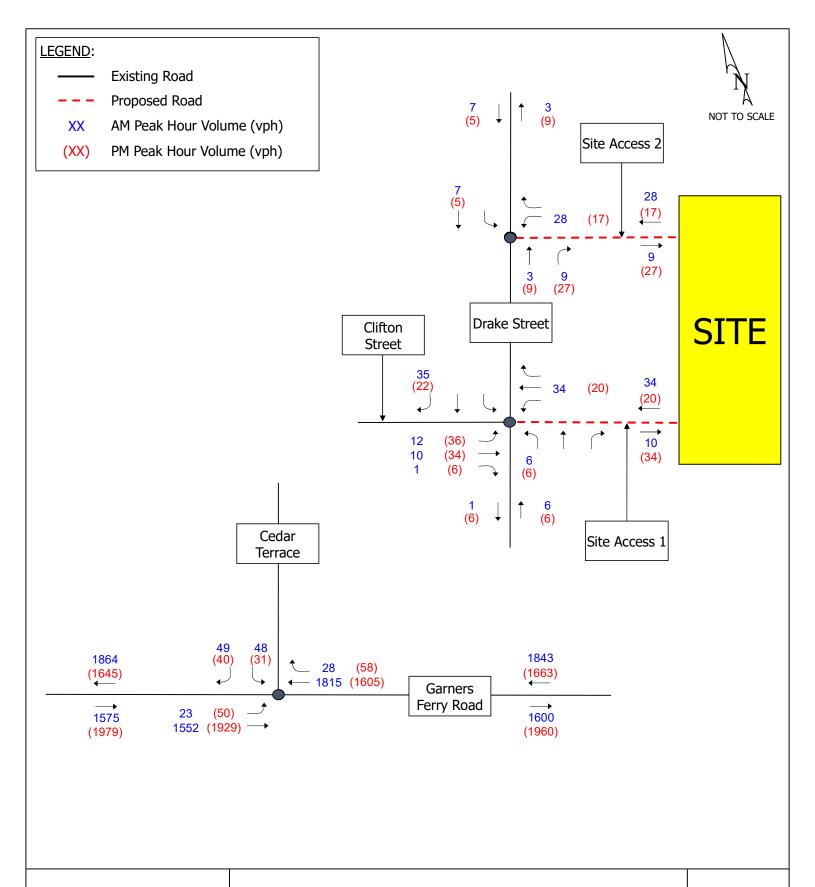
All Drake Street / Clifton Street / Site Access 1 unsignalized intersection approaches are projected to operate at a LOS A during both 2023 Build peak hours. As described in **Section 2**, this intersection was analyzed as an all-way Stop Control intersection. The developer should coordinate with the City to ensure proper intersection control signage at this location. No geometric improvements are recommended due to the construction of the subject development.

All Drake Street / Site Access 2 unsignalized intersection approaches are projected to operate at a LOS A during both 2023 Build peak hours. No improvements are recommended due to the construction of the subject development.

Table 5-1: Intersection Level of Service and Delay Summary 2023 Build Traffic Volumes

		AM PEAR	HOUR	PM PEAK HOUR		
Intersection	Movement and Approach	Delay ¹ (sec/veh)	LOS 1	Delay ¹ (sec/veh)	LOS 1	
1: Garners Ferry Road & Ceder Terrace Street	EB Approach	0.6	Α	1.1	Α	
	WB Approach	0.0	Α	0.0	Α	
	SB Approach	753.0	F	557.5	F	
2: Drake Street & Clifton Street / Site Access 1	EB Approach	7.2	Α	7.6	Α	
	WB Approach	7.3	Α	7.2	Α	
	NB Approach	7.1	Α	7.2	Α	
	SB Approach	6.8	Α	6.9	Α	
	Overall	7.1	Α	7.3	Α	
3: Drake Street & Site Access 2	WB Approach	8.7	Α	8.7	Α	
	NB Approach	0.0	Α	0.0	Α	
	SB Approach	2.6	Α	3.2	Α	

¹ Overall intersection LOS and delay not reported for TWSC intersections.





Drake Street Traffic Impact Analysis2023 Build Traffic Volumes

Figure 5-1

6 CONCLUSIONS AND RECOMMENDATIONS

Capacity analyses were performed for the following scenarios:

- 2022 Existing traffic volumes
- 2023 Background traffic volumes
- 2023 Build traffic volumes (Background + site trips)

In closing, no improvements are recommended in conjunction with the construction of the proposed development.

Appendix A – Scoping Information

Cliff Lawson

From: Brewer, David D < David.Brewer@columbiasc.gov>

Sent: Friday, August 12, 2022 6:58 AM

To: Cliff Lawson
Cc: Jeff Hochanadel

Subject: Re: [EXTERNAL] 1002 Drake Street (Drake Street Residential) TIA

CAUTION: This email originated from outside of the organization. Do not click links or open attachments unless you recognize the sender and know the content is safe.

The standards in the SCDOT ARMS manual will be fine for the TIA.

From: Cliff Lawson < Cliff.Lawson@timmons.com>

Sent: Thursday, August 11, 2022 5:01 PM

To: Brewer, David D **Cc:** Jeff Hochanadel

Subject: [EXTERNAL] 1002 Drake Street (Drake Street Residential) TIA

CAUTION: This email originated outside of the organization. Do not click links or open attachments from unknown senders or suspicious emails. Never enter a username or password on a site that you did not knowingly access.

Mr. Brewer,

Thanks for taking the time to meet with us today. Below is an outline of what was discussed in today's meeting. Hopefully this will suffice for scoping purposes. Please comment as you see fit.

- Building Program: 150 multi-family units → Trips will be generated per the ITE Trip Generation Manual, 11th
 Edition
- Build-out Year: 2023
- Study Area Intersections:
 - o Garners Ferry Road / Cedar Terrace
 - Drake Street / Clifton Street / Site Access 1
 - Drake Street / Site Access 2 → After discussing internally, it was determined that Site Access 2 will be approximately 150-feet south of Norris Street so SCDOT will not need to be involved.
- Counts to be conducted the week of August 23rd
 - Either Tuesday, Wednesday, or Thursday
 - o 7-9am and 4-6 pm
- Approved Developments: Assumed none → Will confirm with Planning & Development Services
- Public Improvement Projects: None
- Growth Rate: 2% (Per Garner Ferry Road Historical AADTs)

Also, I was not able to locate any TIA standards for the City. Are there any available or should I just refer to the ARMS manual?

Thanks,

Cliff Lawson, PE, PTOE

Senior Project Manager

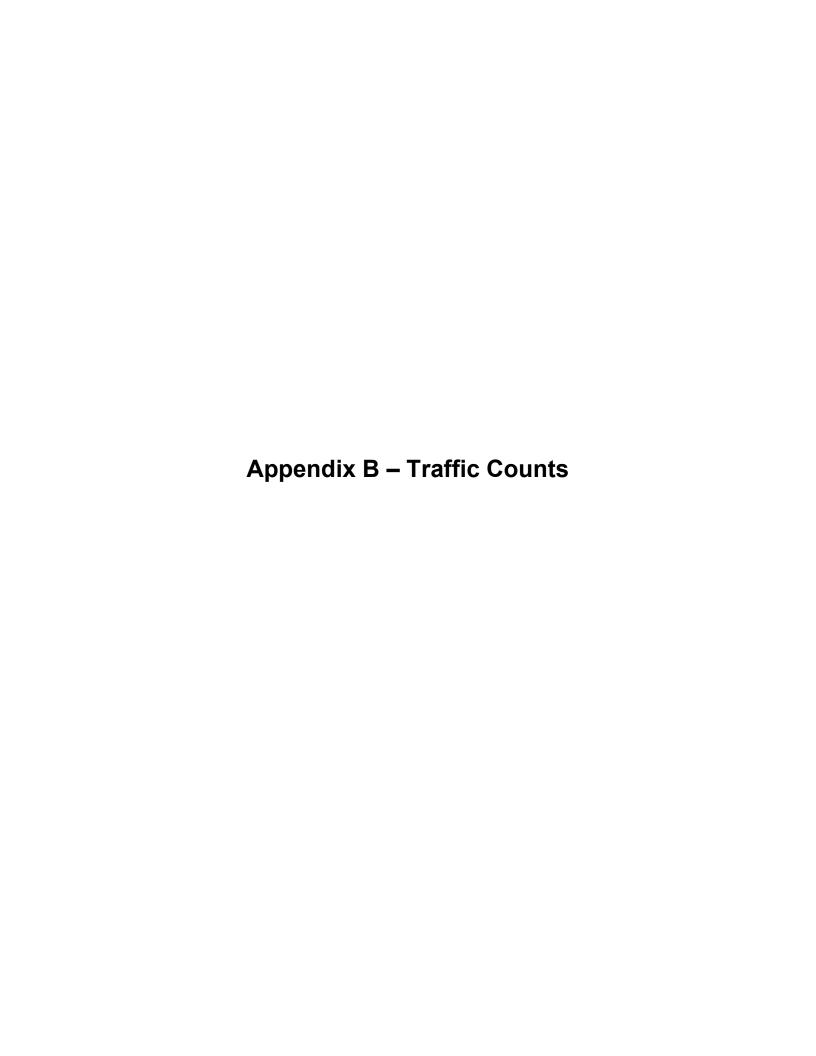
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To send me files greater than 20MB click here.





Site Code:

Start Date : 8/23/2022

Page No : 1

Groups Printed- Cars + - Trucks

	Drake Street Private Access Drake Street Clifton Street																
		Drake	Street			Private	Acces	S		Drake	Street						
		South	bound			West	bound			North	bound		Eastbound				
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
07:00 AM	3	0	0	3	0	0	0	0	0	0	2	2	0	0	0	0	5
07:15 AM	2	0	0	2	0	0	0	0	0	0	1	1	0	0	1	1	4
07:30 AM	1	0	0	1	0	0	0	0	0	0	1	1	0	0	2	2	4
07:45 AM	1	0	0	1	0	0	0	0	0	0	2	2	1	0	0	1	4_
Total	7	0	0	7	0	0	0	0	0	0	6	6	1	0	3	4	17
08:00 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	1
08:15 AM	2	0	0	2	0	0	0	0	0	0	1	1	0	0	1	1	4
08:30 AM	3	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	3
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0_
Total	5	0	0	5	0	0	0	0	0	0	2	2	0	0	1	1	8
Grand Total	12	0	0	12	0	0	0	0	0	0	8	8	1	0	4	5	25
Apprch %	100	0	0		0	0	0		0	0	100		20	0	80		
Total %	48	0	0	48	0	0	0	0	0	0	32	32	4	0	16	20	
Cars +	12	0	0	12	0	0	0	0	0	0	8	8	1	0	4	5	25
% Cars +	100	0	0	100	0	0	0	0	0	0	100	100	100	0	100	100	100_
Trucks	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% Trucks	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

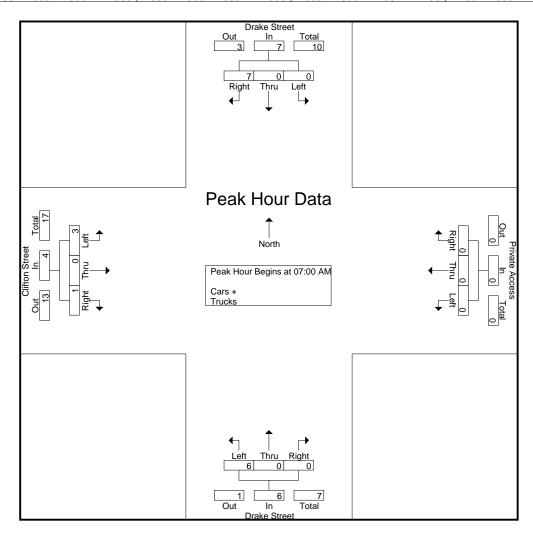


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		Drake Street Private Access								Drake	Street						
		South	bound			Westl	oound			North	bound						
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
Peak Hour Ana	alysis Fro	om 07:0	0 AM to	o 08:45 A	M - Pea	ık 1 of 1			_				_				
Peak Hour for I	Entire In	tersection	on Beg	ins at 07:	00 AM												
07:00 AM	3	0	0	3	0	0	0	0	0	0	2	2	0	0	0	0	5
07:15 AM	2	0	0	2	0	0	0	0	0	0	1	1	0	0	1	1	4
07:30 AM	1	0	0	1	0	0	0	0	0	0	1	1	0	0	2	2	4
07:45 AM	1	0	0	1	0	0	0	0	0	0	2	2	1	0	0	1	4
Total Volume	7	0	0	7	0	0	0	0	0	0	6	6	1	0	3	4	17
% App. Total	100	0	0		0	0	0		0	0	100		25	0	75		
PHF	.583	.000	.000	.583	.000	.000	.000	.000	.000	.000	.750	.750	.250	.000	.375	.500	.850





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Groups Printed- Cars + - Trucks

	Drake Street Private Access Drake Street Clifton Street																
		Drake	Street			Private	Acces	S		Drake	Street			Clifton Street			
		South	bound			West	bound			North	nbound			Eastl	bound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
04:00 PM	1	0	0	1	0	0	0	0	0	0	1	1	1	0	0	1	3
04:15 PM	0	0	0	0	0	0	0	0	0	0	1	1	1	0	0	1	2
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	1	0	2	3	3
04:45 PM	1	0	0	1	0	0	0	0	0	0	1	1	2	0	0	2	4
Total	2	0	0	2	0	0	0	0	0	0	3	3	5	0	2	7	12
05:00 PM	0	0	0	0	0	0	0	0	۱ 0	0	2	2	1	٥	2	3	5
05:15 PM	3	0	0	3	0	0	0	0	0	0	1	1	2	0	2	5	٥
05:30 PM	1	0	0	1	0	0	0	0	0	0	3	3	1	0	1	2	6
05:45 PM		0	0	1	0	0	0	0	0	0	0	0	1	0	1	5	6
Total	5	0	0	5	0	0	0	0	0	0	6	6	6	0	9	15	26
Total	3	U	U	3	, 0	U	U	U	, 0	U	U	U	, 0	U	3	13	20
Grand Total	7	0	0	7	0	0	0	0	0	0	9	9	11	0	11	22	38
Apprch %	100	0	0		0	0	0		0	0	100		50	0	50		
Total %	18.4	0	0	18.4	0	0	0	0	0	0	23.7	23.7	28.9	0	28.9	57.9	
Cars +	7	0	0	7	0	0	0	0	0	0	9	9	11	0	11	22	38
% Cars +	100	0	0	100	0	0	0	0	0	0	100	100	100	0	100	100	100
Trucks	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
% Trucks	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

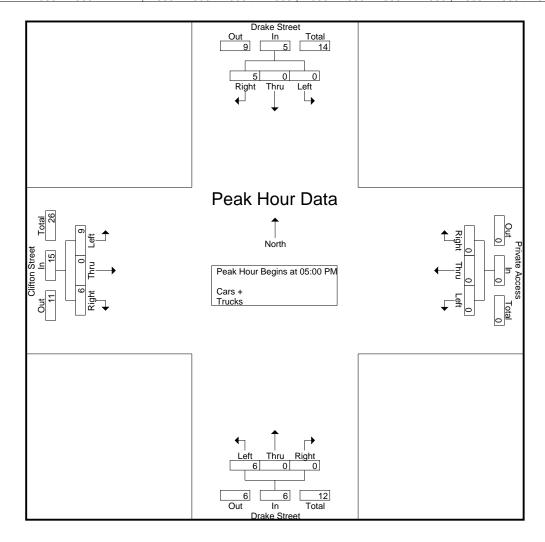


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		Drake	Street		Drake Street Private Access									Drake Street Clifton Street							
		South	bound			Westh	ound		Northbound				Eastbound								
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total				
Peak Hour Ana	lysis Fro	om 04:0	0 PM t	o 05:45 P	M - Pea	k 1 of 1															
Peak Hour for I	Entire In	tersecti	on Beg	ins at 05:	00 PM																
05:00 PM	0	0	0	0	0	0	0	0	0	0	2	2	1	0	2	3	5				
05:15 PM	3	0	0	3	0	0	0	0	0	0	1	1	3	0	2	5	9				
05:30 PM	1	0	0	1	0	0	0	0	0	0	3	3	1	0	1	2	6				
05:45 PM	1	0	0	1	0	0	0	0	0	0	0	0	1	0	4	5	6				
Total Volume	5	0	0	5	0	0	0	0	0	0	6	6	6	0	9	15	26				
% App. Total	100	0	0		0	0	0		0	0	100		40	0	60						
PHF	.417	.000	.000	.417	.000	.000	.000	.000	.000	.000	.500	.500	.500	.000	.563	.750	.722				





File Name: Columbia(Garners Ferry and Cedar Terrace)1190

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Groups Printed- Cars + - Trucks

				Houps Printe	u- Cais + -	TTUCKS			1	
	Garners Ferry Road			Cedar Terrace			Garners Ferry Road			
	Southbound			Westbound			Northbound			
Start Time	Thru	Left	App. Total	Right	Left	App. Total	Right	Thru	App. Total	Int. Total
07:00 AM	234	4	238	10	3	13	0	387	387	638
07:15 AM	353	2	355	6	4	10	3	455	458	823
07:30 AM	397	5	402	1	7	8	3	458	461	871
07:45 AM	390	3	393	7	3	10	5	453	458	861
Total	1374	14	1388	24	17	41	11	1753	1764	3193
08:00 AM	315	4	319	4	3	7	7	388	395	721
08:15 AM	277	0	277	4	3	7	4	431	435	719
08:30 AM	237	1	238	8	3	11	4	358	362	611
08:45 AM	239	0	239	2	3	5	5	362	367	611
Total	1068	5	1073	18	12	30	20	1539	1559	2662
Grand Total	2442	19	2461	42	29	71	31	3292	3323	5855
Apprch %	99.2	0.8		59.2	40.8		0.9	99.1		
Total %	41.7	0.3	42	0.7	0.5	1.2	0.5	56.2	56.8	
Cars +	2379	18	2397	42	28	70	30	3239	3269	5736
% Cars +	97.4	94.7	97.4	100	96.6	98.6	96.8	98.4	98.4	98
 Trucks	63	1	64	0	1	1	1	53	54	119
% Trucks	2.6	5.3	2.6	0	3.4	1.4	3.2	1.6	1.6	2



TRAFFIC DATA COLLECTION

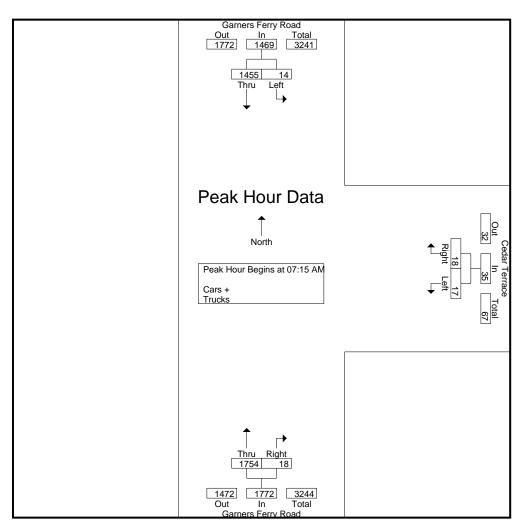
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	Garners Ferry Road Southbound			Cedar Terrace Westbound			Garners Ferry Road Northbound			
Start Time	Thru	Left	App. Total	Right	Left	App. Total	Right	Thru	App. Total	Int. Total
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1										
Peak Hour for Entire Intersection Begins at 07:15 AM										
07:15 AM	353	2	355	6	4	10	3	455	458	823
07:30 AM	397	5	402	1	7	8	3	458	461	871
07:45 AM	390	3	393	7	3	10	5	453	458	861
MA 00:80	315	4	319	4	3	7	7	388	395	721
Total Volume	1455	14	1469	18	17	35	18	1754	1772	3276
% App. Total	99	11		51.4	48.6		1	99		
PHF	.916	.700	.914	.643	.607	.875	.643	.957	.961	.940





File Name: Columbia(Garners Ferry and Cedar Terrace)1190

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Groups Printed- Cars + - Trucks

			G	roups Printed	- Cars + -	Trucks				
	Garners Ferry Road			Cedar Terrace			Garners Ferry Road			
	5	Southbound	d l	Westbound			Northbound			
Start Time	Thru	Left	App. Total	Right	Left	App. Total	Right	Thru	App. Total	Int. Total
04:00 PM	425	2	427	5	3	8	5	392	397	832
04:15 PM	418	3	421	8	6	14	7	388	395	830
04:30 PM	443	6	449	7	6	13	6	406	412	874
 04:45 PM	446	4	450	3	3	6	5	374	379	835
Total	1732	15	1747	23	18	41	23	1560	1583	3371
05:00 PM	449	8	457	3	3	6	3	401	404	867
05:15 PM	473	3	476	7	7	14	10	339	349	839
05:30 PM	491	5	496	8	0	8	8	392	400	904
 05:45 PM	425	10	435	9	3	12	6	335	341	788
Total	1838	26	1864	27	13	40	27	1467	1494	3398
Grand Total	3570	41	3611	50	31	81	50	3027	3077	6769
Apprch %	98.9	1.1		61.7	38.3		1.6	98.4		
 Total %	52.7	0.6	53.3	0.7	0.5	1.2	0.7	44.7	45.5	
Cars +	3531	41	3572	50	31	81	49	2999	3048	6701
 % Cars +	98.9	100	98.9	100	100	100	98	99.1	99.1	99
Trucks	39	0	39	0	0	0	1	28	29	68
% Trucks	1.1	0	1.1	0	0	0	2	0.9	0.9	1



TRAFFIC DATA COLLECTION

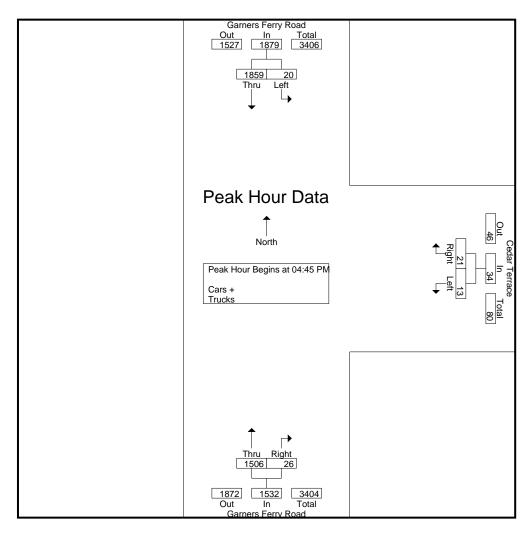
File Name: Columbia(Garners Ferry and Cedar Terrace)1190

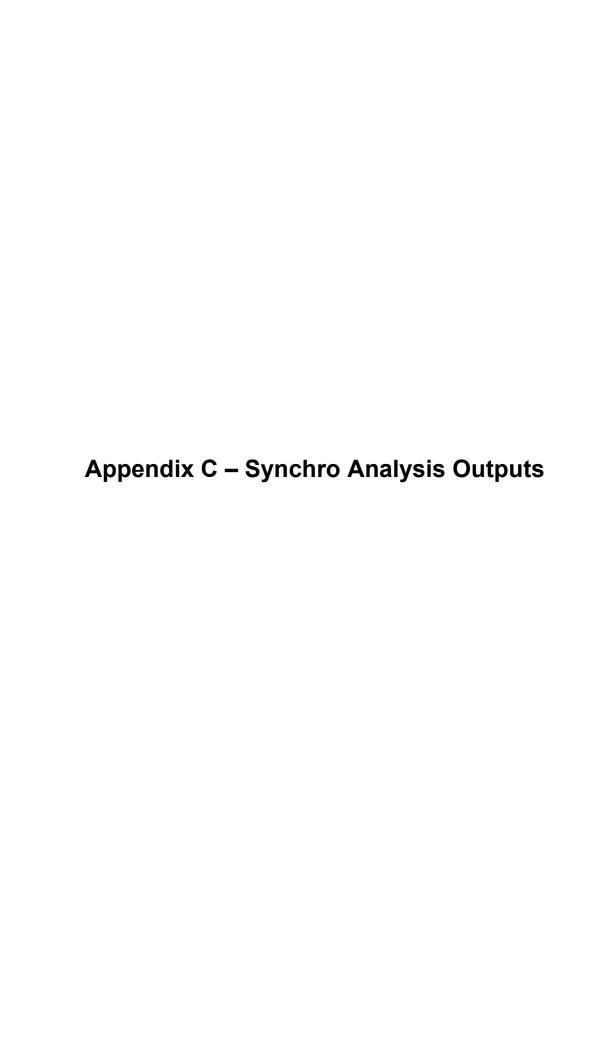
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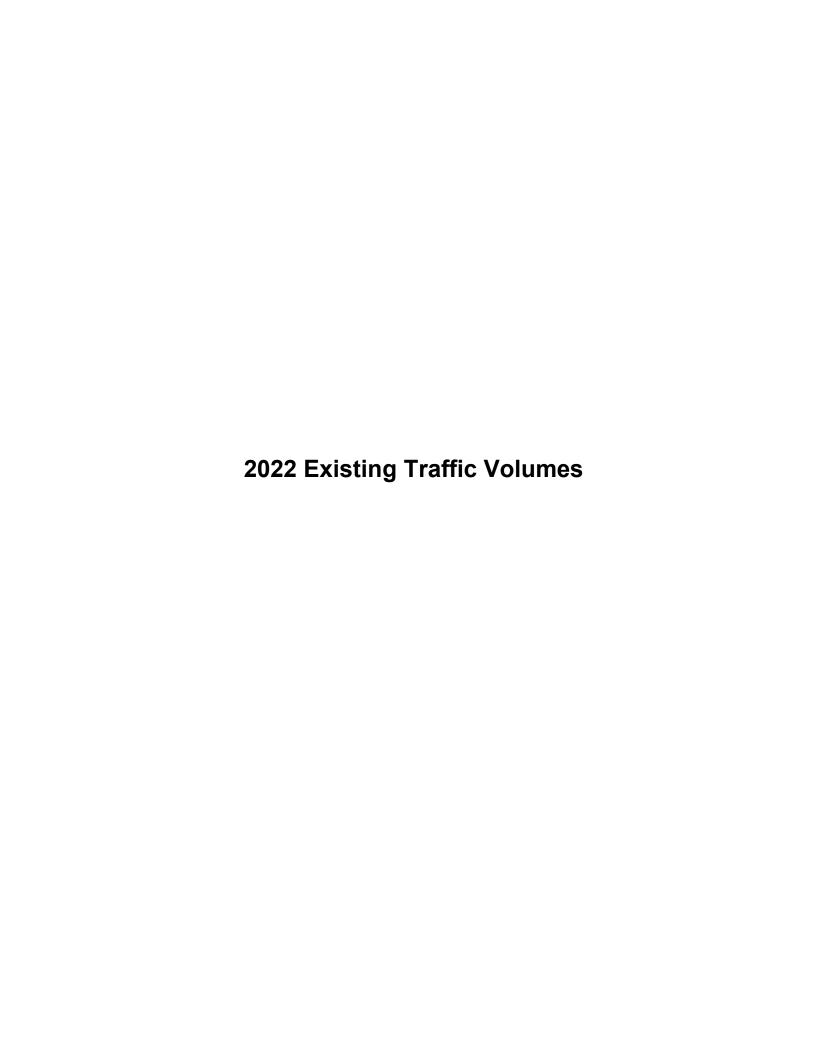
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	Garners Ferry Road Southbound			Cedar Terrace Westbound			Garners Ferry Road Northbound			
Start Time	Thru	Left	App. Total	Right	Left	App. Total	Right	Thru	App. Total	Int. Total
Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1										
Peak Hour for Entire Intersection Begins at 04:45 PM										
04:45 PM	446	4	450	3	3	6	5	374	379	835
05:00 PM	449	8	457	3	3	6	3	401	404	867
05:15 PM	473	3	476	7	7	14	10	339	349	839
05:30 PM	491	5	496	8	0	8	8	392	400	904
Total Volume	1859	20	1879	21	13	34	26	1506	1532	3445
% App. Total	98.9	1.1		61.8	38.2		1.7	98.3		
PHF	.947	.625	.947	.656	.464	.607	.650	.939	.948	.953







Intersection						
Int Delay, s/veh	1.5					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	7		^	1,51	Y	UDIK
Traffic Vol, veh/h	14	1455	1754	18	17	18
Future Vol, veh/h	14	1455	1754	18	17	18
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-		- Olop	None
Storage Length	200	-	_	-	0	-
Veh in Median Storage		0	0		0	_
Grade, %	, π -	0	0	<u>-</u>	0	<u>-</u>
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mymt Flow	16	1617	1949	20	19	20
IVIVIIIL FIUW	10	1017	1949	20	19	20
Major/Minor N	Major1	ľ	Major2	N	Minor2	
Conflicting Flow All	1969	0			2638	985
Stage 1	-	-	-	-	1959	-
Stage 2	_	_	_	_	679	_
Critical Hdwy	5.34	_	_	_	5.74	7.14
Critical Hdwy Stg 1	- 0.04	_	_	_	6.64	-
Critical Hdwy Stg 2	_	_	_	_	6.04	_
Follow-up Hdwy	3.12	_	_	<u>-</u>	3.82	3.92
Pot Cap-1 Maneuver	130			_	42	212
Stage 1	130	_	_	_	60	- 212
Stage 2			_		423	
Platoon blocked, %	-	_	-	<u>-</u>	423	-
	130	-	-	-	37	212
Mov Cap-1 Maneuver		-			37	
Mov Cap-2 Maneuver	-	-	-	-		-
Stage 1	-	-	-	-	53	-
Stage 2	-	-	-	-	423	-
Approach	EB		WB		SB	
HCM Control Delay, s	0.3		0		125.2	
HCM LOS	3.0				F	
Minor Lane/Major Mvm	t	EBL	EBT	WBT	WBR :	SRI n1
		130	רטו	וטייי	VVDIT (
Capacity (veh/h) HCM Lane V/C Ratio			-	-	-	64
		0.12	-	-		0.608
HCM Control Delay (s)		36.4	-	-	-	
HCM Lane LOS		0.4	-	-	-	F 2.6
HCM 95th %tile Q(veh)						

2022 Existing AM Peak
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ludous office						
Intersection Delay alueb	6.8					
Intersection Delay, s/veh Intersection LOS	6.8 A					
IIILEI SECLIOII LOS	А					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	Y			4	F	
Traffic Vol, veh/h	4	4	6	4	4	7
Future Vol, veh/h	4	4	6	4	4	7
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	4	4	7	4	4	8
Number of Lanes	1	0	0	1	1	0
Approach	EB		NB		SB	
Opposing Approach			SB		NB	
Opposing Lanes	0		1		1	
Conflicting Approach Left	SB		EB			
Conflicting Lanes Left	1		1		0	
Conflicting Approach Right	NB				EB	
Conflicting Lanes Right	1		0		1	
HCM Control Delay	6.8		7.1		6.6	
HCM LOS	Α		Α		Α	
Lane		NBLn1	EBLn1	SBLn1		
Vol Left, %		60%	50%	0%		
Vol Thru, %		40%	0%	36%		
Vol Right, %		0%	50%	64%		
Sign Control		Stop	Stop	Stop		
Traffic Vol by Lane		10	8	11		
LT Vol		6	4	0		
Through Vol		4	0	4		
RT Vol		0	4	7		
Lane Flow Rate		11	9	12		
Geometry Grp		1	1	1		
Degree of Util (X)		0.013	0.009	0.012		
Departure Headway (Hd)		4.079	3.775	3.576		
Convergence, Y/N		Yes	Yes	Yes		
Cap		882	952	1006		
Service Time		2.082	1.783	1.581		
HCM Lane V/C Ratio		0.012	0.009	0.012		
HCM Control Delay		7.1	6.8	6.6		
HCM Lane LOS		Α	Α.	Α		
HCM 95th-tile Q		0	0	0		
		U	U	U		

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Intersection						
Int Delay, s/veh	0.9					
		EDT	WDT	WDD	CDI	SBR
Movement	EBL	EBT	WBT	WBR	SBL	SBK
Lane Configurations	7		4500	00	Y	04
Traffic Vol, veh/h	20	1859	1506	26	13	21
Future Vol, veh/h	20	1859	1506	26	13	21
Conflicting Peds, #/hr	0	_ 0	_ 0	_ 0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	200	-	-	-	0	-
Veh in Median Storage	, # -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	22	2066	1673	29	14	23
Major/Minor I	Major1		Major2	N	Minor2	
						054
Conflicting Flow All	1702	0	-	0	2558	851
Stage 1	-	-	-	-	1688	-
Stage 2	-	-	-	-	870	-
Critical Hdwy	5.34	-	-	-	5.74	7.14
Critical Hdwy Stg 1	-	-	-	-	6.64	-
Critical Hdwy Stg 2	-	-	-	-	6.04	-
Follow-up Hdwy	3.12	-	-	-	3.82	3.92
Pot Cap-1 Maneuver	177	-	-	-	46	260
Stage 1	-	-	-	-	90	-
Stage 2	-	-	-	-	335	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	177	-	-	_	40	260
Mov Cap-2 Maneuver	-	_	_	_	40	
Stage 1	_	_	_	_	79	_
Stage 2	_	_	_	_	335	_
Olage 2					000	
Approach	EB		WB		SB	
HCM Control Delay, s	0.3		0		79	
HCM LOS					F	
Minor Long /Maior P4		EDI	EDT	WDT	MDD	2DL 4
Minor Lane/Major Mvm	It	EBL	EBT	WBT	WBR :	
Capacity (veh/h)		177	-	-	-	84
HCM Lane V/C Ratio		0.126	-	-	-	0.45
HCM Control Delay (s)		28.2	-	-	-	79
HCM Lane LOS		D	-	-	-	F
HCM 95th %tile Q(veh)	1	0.4	_	_	_	1.9
ICIVI 95til 76tile Q(Vell)	1	0.7				1.0

2022 Existing PM Peak
Timmons Group
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Intersection						
Intersection Delay, s/veh	6.9					
Intersection LOS	0.9 A					
III.O. JOOLIOIT EOO						
Mayamant	EDI	EDD	NDI	NDT	CDT	CDD
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	M	•	^	स	Þ	_
Traffic Vol, veh/h	9	6	6	4	4	5
Future Vol, veh/h	9	6	6	4	4	5
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	10	7	7	4	4	6
Number of Lanes	1	0	0	1	1	0
Approach	EB		NB		SB	
Opposing Approach			SB		NB	
Opposing Lanes	0		1		1	
Conflicting Approach Left	SB		EB			
Conflicting Lanes Left	1		1		0	
Conflicting Approach Right	NB				EB	
Conflicting Lanes Right	1		0		1	
HCM Control Delay	6.9		7.2		6.7	
HCM LOS	Α		Α		Α	
Lane		NBLn1	EBLn1	SBLn1		
Vol Left, %		60%	60%	0%		
Vol Thru, %		40%	0%	44%		
Vol Right, %		0%	40%	56%		
Sign Control		Stop	Stop	Stop		
Traffic Vol by Lane		10	15	9		
LT Vol		6	9	0		
Through Vol		4	0	4		
RT Vol		0	6	5		
Lane Flow Rate		11	17	10		
Geometry Grp		1	1	1		
Degree of Util (X)		0.013	0.018	0.01		
Departure Headway (Hd)		4.091	3.851	3.639		
Convergence, Y/N		Yes	Yes	Yes		
Cap		879	933	987		
Service Time		2.098	1.859	1.647		
HCM Lane V/C Ratio		0.013	0.018	0.01		
HCM Control Delay		7.2	6.9	6.7		
HCM Lane LOS		Α.Δ	Α	Α		
HCM 95th-tile Q		0	0.1	0		
HOW JOHNIE Q		U	0.1	U		

2022 Existing PM Peak
Timmons Group
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2023 Background Traffic	c Volumes

Intersection						
Int Delay, s/veh	1.8					
		EDT	WDT	WDD	CDI	CDD
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations			*	40	Y	.10
Traffic Vol, veh/h	14	1552	1815	18	17	18
Future Vol, veh/h	14	1552	1815	18	17	18
Conflicting Peds, #/hr	_ 0	_ 0	_ 0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	200	-	-	-	0	-
Veh in Median Storage,	# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	16	1724	2017	20	19	20
Major/Minor M	lajor1		Major?		Minor2	
			Major2			1010
	2037	0	-	0	2749	1019
Stage 1	-	-	-	-	2027	-
Stage 2	-	-	-	-	722	-
Critical Hdwy	5.34	-	-	-	5.74	7.14
Critical Hdwy Stg 1	-	-	-	-	6.64	-
Critical Hdwy Stg 2	-	-	-	-	6.04	-
Follow-up Hdwy	3.12	-	-	-	3.82	3.92
Pot Cap-1 Maneuver	120	-	-	-	36	201
Stage 1	-	-	-	-	55	-
Stage 2	-	-	-	-	402	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	120	-	-	-	31	201
Mov Cap-2 Maneuver	-	-	-	-	31	-
Stage 1	-	-	_	-	48	-
Stage 2	_	-	_	_	402	_
- 11-13-2						
			14.75		0.5	
Approach	EB		WB		SB	
HCM Control Delay, s	0.4		0		163.2	
HCM LOS					F	
Minor Lane/Major Mvmt		EBL	EBT	WBT	WBR :	SBI n1
Capacity (veh/h)		120	LDI	-	- 1001	55
HCM Lane V/C Ratio		0.13	-	-		0.707
HCM Control Delay (s)		39.4	_	-		163.2
HOW CONTROL DEIGN (S)				_		
HCM Lane LOS HCM 95th %tile Q(veh)		0.4	-	-	-	F 2.9

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Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 4 RT Vol 0 4 7 1 Lane Flow Rate 11 9 12 1 1 Geometry Grp 1 1 1 1 1 1 Departure Headway (Hd) 4.079 3.775 3.576 2 2 0 0 4 7 2 0	Interception						
Novement		6.0					
Movement							
Traffic Vol, veh/h	IIIIGI 3GUIUII LU3	A					
Traffic Vol, veh/h							
Traffic Vol, veh/h 4 4 6 4 4 7 Future Vol, veh/h 4 4 6 4 4 7 Peak Hour Factor 0.90 0.			EBR	NBL			SBR
Future Vol, veh/h 4 4 6 4 4 7 Peak Hour Factor 0.90		Y			र्स	Þ	
Peak Hour Factor 0.90							
Heavy Vehicles, %							
Mvmt Flow 4 4 7 4 4 8 Number of Lanes 1 0 0 1 1 0 Approach EB NB SB NB Opposing Approach SB NB NB Opposing Lanes 0 1 1 1 Conflicting Approach Left SB EB Conflicting Lanes Left 1 0							
Number of Lanes 1 0 0 1 1 0 Approach EB NB SB Opposing Approach SB NB Opposing Lanes 0 1 1 Conflicting Approach Left SB EB Conflicting Lanes Left 1 1 0 Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Right, % 60% 50% 0% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 4 RT Vol 0 4 7 1 Lane Flow Rate 11 9 <							
Approach EB NB SB Opposing Approach SB NB Opposing Lanes 0 1 1 Conflicting Approach Left SB EB Conflicting Lanes Left 1 0 Conflicting Approach Right NB EB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A A A Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometr		4			4	4	
Opposing Approach SB NB Opposing Lanes 0 1 1 Conflicting Approach Left SB EB Conflicting Lanes Left 1 1 0 Conflicting Approach Right NB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 <	Number of Lanes	1	0	0	1	1	0
Opposing Lanes 0 1 1 Conflicting Approach Left SB EB Conflicting Lanes Left 1 1 0 Conflicting Approach Right NB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 50% 64% 50m 64% Sign Control Stop Stop Stop Stop Traffic Vol by Lane 10 8 11 11 11 LT Vol 6 4 0 4 7 1 4 0 4 7 1 1 1 1 1 1 1 2 2 2 1 <td>Approach</td> <td>EB</td> <td></td> <td>NB</td> <td></td> <td>SB</td> <td></td>	Approach	EB		NB		SB	
Opposing Lanes 0 1 1 Conflicting Approach Left SB EB Conflicting Lanes Left 1 1 0 Conflicting Approach Right NB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 60% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 4 RT Vol 4 0 4 7 Lane Flow Rate 11 9 12 1 Geometry Grp 1 1 1 1				SB		NB	
Conflicting Approach Left SB EB Conflicting Lanes Left 1 1 0 Conflicting Approach Right NB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 <td></td> <td>0</td> <td></td> <td>1</td> <td></td> <td>1</td> <td></td>		0		1		1	
Conflicting Lanes Left 1 1 0 Conflicting Approach Right NB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N		SB		EB			
Conflicting Approach Right NB EB Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882<		1		1		0	
Conflicting Lanes Right 1 0 1 HCM Control Delay 6.8 7.1 6.6 HCM LOS A A A A A A A Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 4 Through Vol 4 0 4 7 Lane Flow Rate 11 9 12 1 1 Geometry Grp 1 1 1 1 1 1 1 2 2 2 2 1 2 3.576 2 2 2 2 2 2 2 2 2 2 2 2 2 </td <td></td> <td>NB</td> <td></td> <td></td> <td></td> <td>EB</td> <td></td>		NB				EB	
HCM Control Delay 6.8 7.1 6.6 HCM LOS A		1		0		1	
Lane NBLn1 EBLn1 SBLn1 Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6	HCM Control Delay	6.8		7.1		6.6	
Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A		Α		Α		Α	
Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Vol Left, % 60% 50% 0% Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A	Lane		NBLn1	EBLn1	SBLn1		
Vol Thru, % 40% 0% 36% Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Vol Right, % 0% 50% 64% Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Sign Control Stop Stop Stop Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Traffic Vol by Lane 10 8 11 LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
LT Vol 6 4 0 Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Through Vol 4 0 4 RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A	LT Vol						
RT Vol 0 4 7 Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Lane Flow Rate 11 9 12 Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Geometry Grp 1 1 1 Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Degree of Util (X) 0.013 0.009 0.012 Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
Departure Headway (Hd) 4.079 3.775 3.576 Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A			0.013	0.009	0.012		
Convergence, Y/N Yes Yes Yes Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A			4.079	3.775	3.576		
Cap 882 952 1006 Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A	Convergence, Y/N				Yes		
Service Time 2.082 1.783 1.581 HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
HCM Lane V/C Ratio 0.012 0.009 0.012 HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A				1.783			
HCM Control Delay 7.1 6.8 6.6 HCM Lane LOS A A A							
HCM Lane LOS A A A							
110N 3501-00 Q U U U	HCM 95th-tile Q		0	0	0		

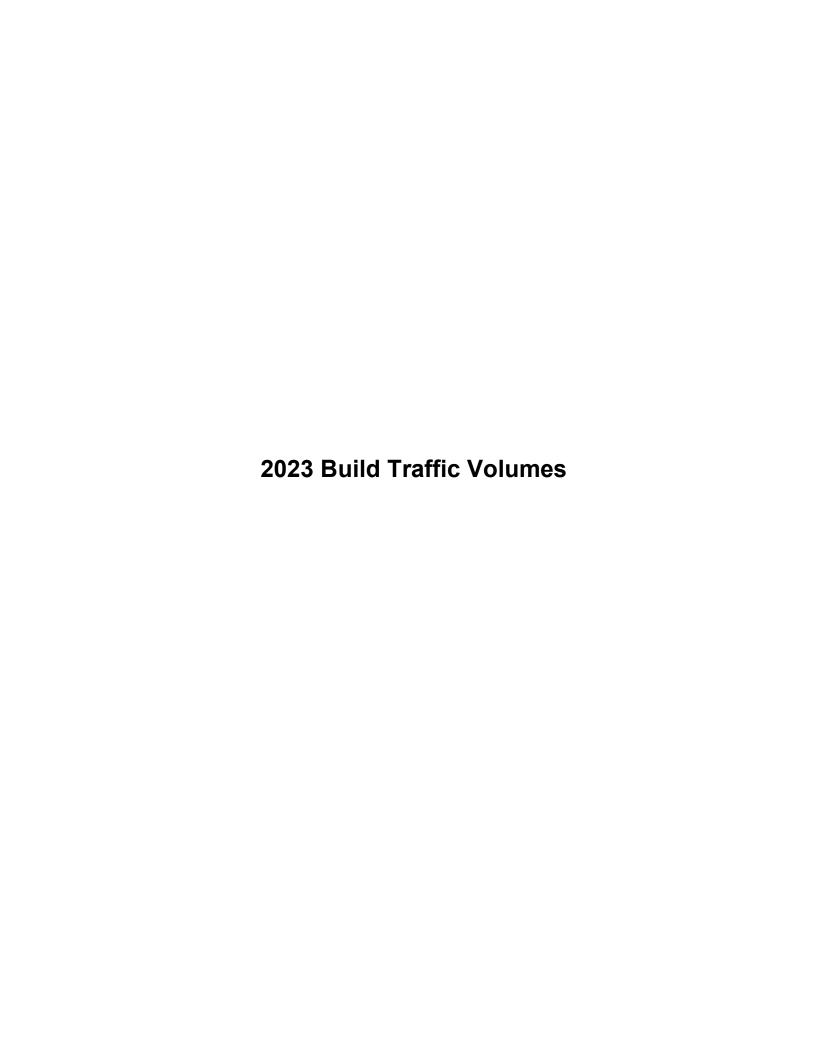
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Intersection						
Int Delay, s/veh	1.1					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	7		ተተጉ		Y	
Traffic Vol, veh/h	20	1929	1605	27	13	21
Future Vol, veh/h	20	1929	1605	27	13	21
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-		-	None
Storage Length	200	-	-	-	0	-
Veh in Median Storage,		0	0	_	0	_
Grade, %	_	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	22	2143	1783	30	14	23
NA ' (NA' N					4: 0	
	/lajor1		Major2		Minor2	
Conflicting Flow All	1813	0	-	0	2699	907
Stage 1	-	-	-	-	1798	-
Stage 2	-	-	-	-	901	-
Critical Hdwy	5.34	-	-	-	5.74	7.14
Critical Hdwy Stg 1	-	-	-	-	6.64	-
Critical Hdwy Stg 2	-	-	-	-	6.04	-
Follow-up Hdwy	3.12	-	-	-	3.82	3.92
Pot Cap-1 Maneuver	155	-	-	-	39	239
Stage 1	-	-	-	-	77	-
Stage 2	-	-	-	-	323	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	155	-	-	-	33	239
Mov Cap-2 Maneuver	-	-	-	-	33	-
Stage 1	-	-	_	-	66	-
Stage 2	_	-	_	_	323	-
g v =						
Approach	EB		WB		SB	
HCM Control Delay, s	0.3		0		102.8	
HCM LOS					F	
Minor Lane/Major Mvm		EBL	EBT	WBT	WBR :	SBLn1
Capacity (veh/h)		155	-		-	71
HCM Lane V/C Ratio		0.143	_	_		0.532
HCM Control Delay (s)		32.1	_	-	_	
HCM Lane LOS		32.1 D	-	-	-	102.6 F
HCM 95th %tile Q(veh)		0.5	_	-		2.2
HOW SOUT WILLE Q(Ven)		0.5	-	-	-	2.2

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Intersection						
Intersection Delay, s/veh	6.9					
Intersection LOS	0.9 A					
Intersection Loo						
					0==	055
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	M	_	_	स	Þ	-
Traffic Vol, veh/h	9	6	6	4	4	5
Future Vol, veh/h	9	6	6	4	4	5
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	10	7	7	4	4	6
Number of Lanes	1	0	0	1	1	0
Approach	EB		NB		SB	
Opposing Approach			SB		NB	
Opposing Lanes	0		1		1	
Conflicting Approach Left	SB		EB			
Conflicting Lanes Left	1		1		0	
Conflicting Approach Right	NB				EB	
Conflicting Lanes Right	1		0		1	
HCM Control Delay	6.9		7.2		6.7	
HCM LOS	Α		Α		Α	
Lane		NBLn1	EBLn1	SBLn1		
Vol Left, %		60%	60%	0%		
Vol Thru, %		40%	0%	44%		
Vol Right, %		0%	40%	56%		
Sign Control		Stop	Stop	Stop		
Traffic Vol by Lane		10	15	9		
LT Vol		6	9	0		
Through Vol		4	0	4		
RT Vol		0	6	5		
Lane Flow Rate		11	17	10		
Geometry Grp		1	1	1		
Degree of Util (X)		0.013	0.018	0.01		
Departure Headway (Hd)		4.091	3.851	3.639		
Convergence, Y/N		Yes	Yes	Yes		
Сар		879	933	987		
Service Time		2.098	1.859	1.647		
HCM Lane V/C Ratio		0.013	0.018	0.01		
11014.0 (1.0.1		7.2	6.9	6.7		
HCM Control Delay		1.2	0.3	0.7		
HCM Control Delay HCM Lane LOS HCM 95th-tile Q		7.2 A	0.5 A 0.1	A		

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Intersection								
Int Delay, s/veh	21							
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	7		444		Y	UDIT		
Traffic Vol, veh/h	23	1552	1815	28	48	49		
Future Vol, veh/h	23	1552	1815	28	48	49		
Conflicting Peds, #/hr	0	0	0	0	0	0		
Sign Control	Free	Free	Free	Free	Stop	Stop		
RT Channelized	-			None	- Clop	None		
Storage Length	200	-	_	-	0	-		
Veh in Median Storage		0	0	_	0	_		
Grade, %	- -	0	0	_	0	_		
Peak Hour Factor	90	90	90	90	90	90		
Heavy Vehicles, %	2	2	2	2	2	2		
Mymt Flow	26	1724	2017	31	53	54		
IVIVIII I IOW	20	1127	2011	UI	- 55	J 1		
Major/Minor	Major1		Major2		Minor2			
Conflicting Flow All	2048	0	-	0	2775	1024		
Stage 1	2040	-	_	-	2033	1024		
Stage 2		-	_	_	742	_		
Critical Hdwy	5.34	_	_	_	5.74	7.14		
Critical Hdwy Stg 1	J.J4		-	<u>-</u>	6.64	7.14		
Critical Hdwy Stg 2	-	-		-	6.04			
Follow-up Hdwy	3.12	_	_	_	3.82	3.92		
Pot Cap-1 Maneuver	118	-		-	~ 35	200		
Stage 1	110	-	_	_	54	200		
Stage 1	-	_	_	_	392	_		
Platoon blocked, %		_	_	_	332	_		
Mov Cap-1 Maneuver	118	-		_	~ 27	200		
Mov Cap-1 Maneuver	110	-	-	-	~ 27	200		
Stage 1	-	-	-	-	~ 42			
Stage 2	-		-	-	392	_		
Slaye 2	-	-	<u>-</u>	<u>-</u>	332	-		
Approach	EB		WB		SB			
HCM Control Delay, s	0.6		0		\$ 753			
HCM LOS	0.0		U		ψ 733 F			
TION LOO					·			
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR	SBLn1		
Capacity (veh/h)		118			-	48		
HCM Lane V/C Ratio		0.217	_	-		2.245		
HCM Control Delay (s)		43.8	_	_		\$ 753		
HCM Lane LOS		+5.0 E	_	_	_	F		
HCM 95th %tile Q(veh)	0.8	_	_	-	11.1		
Notes	,							
	naoit :	¢. D.	Nov. sv:	0000	200	C	outotion Not Defined	*. All major values in alata
~: Volume exceeds ca	pacity	\$: De	elay exc	eeds 3	JUS	+: Com	outation Not Defined	*: All major volume in plato

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2: Drake Street & Clifton Street/Site Access 1

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Traffic Vol, veh/h	12	10	4	4	34	4	6	4	4	4	4	35
Future Vol, veh/h	12	10	4	4	34	4	6	4	4	4	4	35
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	13	11	4	4	38	4	7	4	4	4	4	39
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	7.2			7.3			7.1			6.8		
HCM LOS	Α			Α			Α			Α		

Lane	NBLn1	EBLn1	WBLn1	SBLn1	
Vol Left, %	43%	46%	10%	9%	
Vol Thru, %	29%	38%	81%	9%	
Vol Right, %	29%	15%	10%	81%	
Sign Control	Stop	Stop	Stop	Stop	
Traffic Vol by Lane	14	26	42	43	
LT Vol	6	12	4	4	
Through Vol	4	10	34	4	
RT Vol	4	4	4	35	
Lane Flow Rate	16	29	47	48	
Geometry Grp	1	1	1	1	
Degree of Util (X)	0.017	0.033	0.052	0.048	
Departure Headway (Hd)	4.015	4.079	4.028	3.606	
Convergence, Y/N	Yes	Yes	Yes	Yes	
Cap	888	877	889	989	
Service Time	2.055	2.106	2.051	1.644	
HCM Lane V/C Ratio	0.018	0.033	0.053	0.049	
HCM Control Delay	7.1	7.2	7.3	6.8	
HCM Lane LOS	Α	Α	Α	Α	
HCM 95th-tile Q	0.1	0.1	0.2	0.2	

2023 Build AM Peak
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Intersection						
Int Delay, s/veh	5.5					
		14/55	Not	NES	051	057
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		Þ			4
Traffic Vol, veh/h	28	4	4	9	4	7
Future Vol, veh/h	28	4	4	9	4	7
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e,# 0	-	0	_	-	0
Grade, %	0	_	0	_	_	0
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	31	4	4	10	4	8
IVIVIIIL FIOW	JI	4	4	10	4	O
Major/Minor	Minor1	N	Major1	ı	Major2	
Conflicting Flow All	25	9	0	0	14	0
Stage 1	9	_	-	_	_	_
Stage 2	16	_	_	_	_	_
Critical Hdwy	6.42	6.22	_	_	4.12	_
Critical Hdwy Stg 1	5.42	0.22		_	4.12	
	5.42		-	-		-
Critical Hdwy Stg 2			-	-	-	-
Follow-up Hdwy	3.518	3.318	-	-	2.218	-
Pot Cap-1 Maneuver	991	1073	-	-	1604	-
Stage 1	1014	-	-	-	-	-
Stage 2	1007	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	988	1073	-	-	1604	-
Mov Cap-2 Maneuver	988	-	-	-	-	-
Stage 1	1014	-	_	-	-	-
Stage 2	1004	_	_	_	_	_
Olago 2	1001					
Approach	WB		NB		SB	
HCM Control Delay, s	8.7		0		2.6	
HCM LOS	Α					
N.4' 1 (N.4. ' N.4.		NDT	NDDV	MDI 4	001	ODT
Minor Lane/Major Mvn	nt	NBT	NBKV	VBLn1	SBL	SBT
Capacity (veh/h)		-	-	000	1604	-
HCM Lane V/C Ratio		-	-	0.036	0.003	-
HCM Control Delay (s))	-	-	8.7	7.3	0
HCM Lane LOS		-	-	Α	Α	Α
HCM 95th %tile Q(veh)	-	-	0.1	0	-

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Intersection								
Int Delay, s/veh	11.2							
Movement	EBL	EBT	WBT	WBR	SBL	SBR		
Lane Configurations	*		ተ ተጉ		Y			
Traffic Vol, veh/h	50	1929	1605	58	31	40		
Future Vol, veh/h	50	1929	1605	58	31	40		
Conflicting Peds, #/hr		0	0	0	0	0		
Sign Control	Free	Free	Free	Free	Stop	Stop		
RT Channelized	_		_	None	_	None		
Storage Length	200	-	-	-	0	-		
Veh in Median Storag	e.# -	0	0	-	0	-		
Grade, %	-	0	0	-	0	-		
Peak Hour Factor	90	90	90	90	90	90		
Heavy Vehicles, %	2	2	2	2	2	2		
Mvmt Flow	56	2143	1783	64	34	44		
Major/Minor	Major1		Major2	N	Minor2			
Conflicting Flow All	1847	0			2784	924		
Stage 1	-	-	-	-	1815	-		
Stage 2	-	_	_	_	969	_		
Critical Hdwy	5.34	_	-	-	5.74	7.14		
Critical Hdwy Stg 1	-	_	_	_	6.64	-		
Critical Hdwy Stg 2	-	-	-	_	6.04	_		
Follow-up Hdwy	3.12	-	-	_	3.82	3.92		
Pot Cap-1 Maneuver	149	-	-	_	35	233		
Stage 1	-	-	-	-	75	-		
Stage 2	-	-	-	-	297	-		
Platoon blocked, %		-	-	-				
Mov Cap-1 Maneuver	149	-	-	-	~ 22	233		
Mov Cap-2 Maneuver		-	-	-	~ 22	-		
Stage 1	-	-	-	-	47	-		
Stage 2	-	-	-	-	297	-		
Approach	EB		WB		SB			
HCM Control Delay, s	1.1		0	\$	557.5			
HCM LOS					F			
Minor Lane/Major Mvr	nt	EBL	EBT	WBT	WBR	SBLn1		
Capacity (veh/h)		149	-	-	-	45		
HCM Lane V/C Ratio		0.373	-	_	_	1.753		
HCM Control Delay (s	3)	42.9	-	_		557.5		
HCM Lane LOS	,	E	-	_	-	F		
HCM 95th %tile Q(veh	۱)	1.6	-	-	-	8		
Notes								
~: Volume exceeds ca	anacity	\$: De	alav evo	eeds 30	າກຣ	+ Com	outation Not Defined	*: All major volume in platoon
. Volume exceeds Ca	μασιιγ	ψ. Dt	ay ext	,cc us 3(000	·. Com	Julation Not Delined	. All major volume in platoon

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2: Drake Street & Clifton Street/Site Access 1

Intersection Delay, s/veh	7.3
Intersection Delay, s/veh Intersection LOS	Α

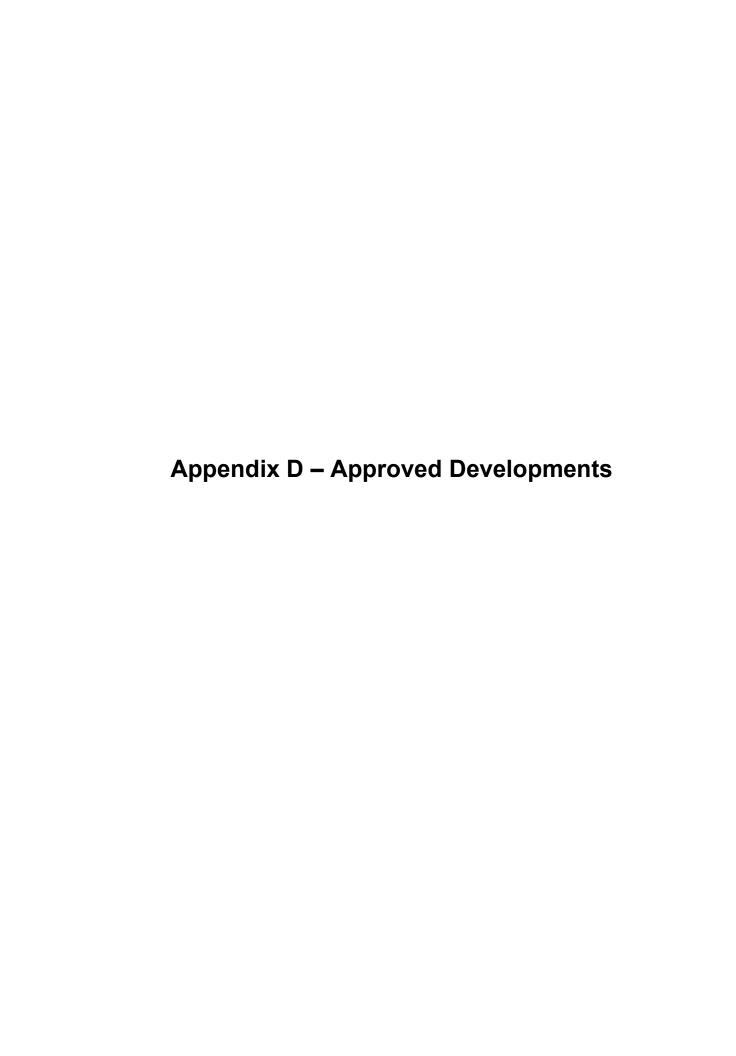
Movement	EBL	EBI	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Traffic Vol, veh/h	36	34	6	4	20	4	6	4	4	4	4	22
Future Vol, veh/h	36	34	6	4	20	4	6	4	4	4	4	22
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	40	38	7	4	22	4	7	4	4	4	4	24
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	7.6			7.2			7.2			6.9		
HCM LOS	Α			Α			Α			Α		

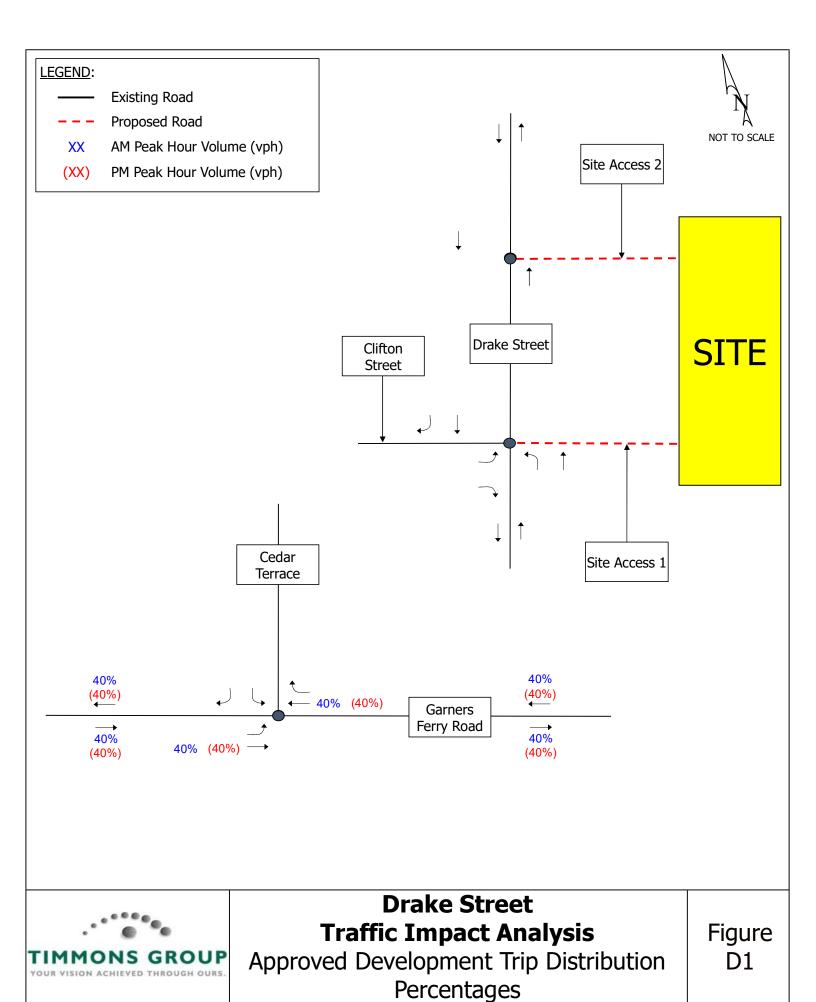
Lane	NBLn1	EBLn1	WBLn1	SBLn1	
Vol Left, %	43%	47%	14%	13%	
Vol Thru, %	29%	45%	71%	13%	
Vol Right, %	29%	8%	14%	73%	
Sign Control	Stop	Stop	Stop	Stop	
Traffic Vol by Lane	14	76	28	30	
LT Vol	6	36	4	4	
Through Vol	4	34	20	4	
RT Vol	4	6	4	22	
Lane Flow Rate	16	84	31	33	
Geometry Grp	1	1	1	1	
Degree of Util (X)	0.018	0.096	0.035	0.035	
Departure Headway (Hd)	4.075	4.091	4.027	3.733	
Convergence, Y/N	Yes	Yes	Yes	Yes	
Cap	871	877	887	950	
Service Time	2.134	2.115	2.062	1.79	
HCM Lane V/C Ratio	0.018	0.096	0.035	0.035	
HCM Control Delay	7.2	7.6	7.2	6.9	
HCM Lane LOS	Α	Α	Α	Α	
HCM 95th-tile Q	0.1	0.3	0.1	0.1	

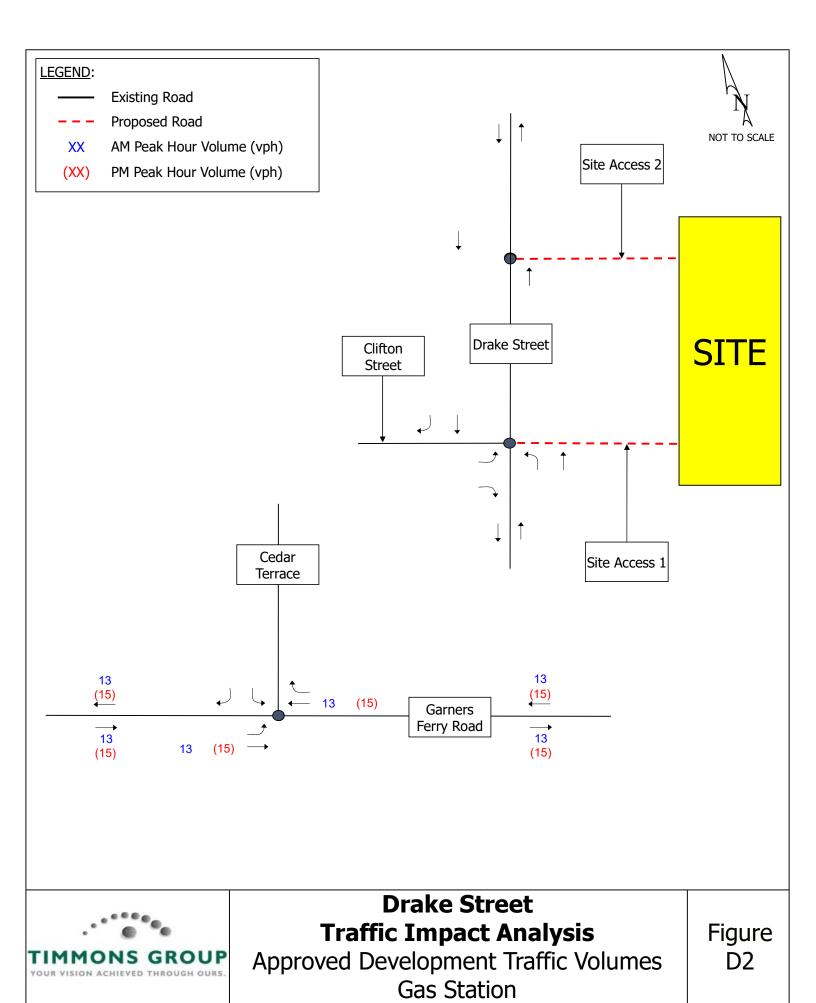
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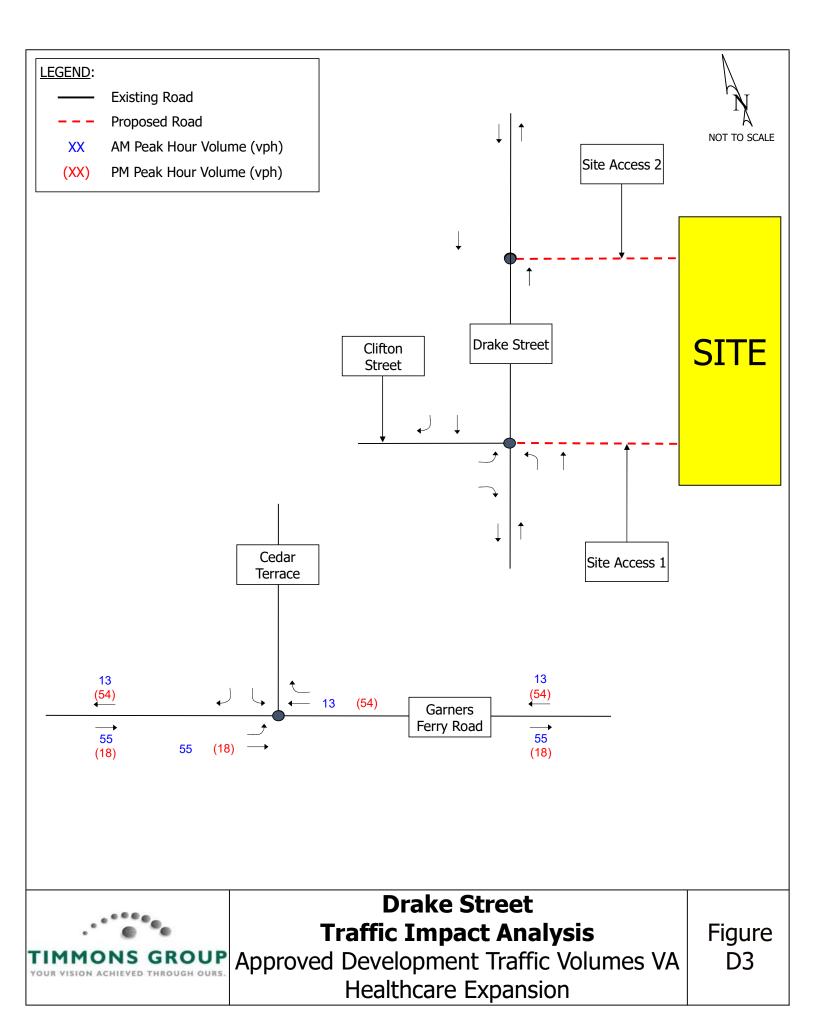
Intersection						
Int Delay, s/veh	3.2					
	WDI	MDD	NDT	NDD	ODI	ODT
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		F			ની
Traffic Vol, veh/h	17	4	9	27	4	5
Future Vol, veh/h	17	4	9	27	4	5
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	_	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage	e,# 0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	19	4	10	30	4	6
WWW.	13	7	10	30		U
Major/Minor	Minor1	N	Major1	I	Major2	
Conflicting Flow All	39	25	0	0	40	0
Stage 1	25	-	-	_	-	-
Stage 2	14	_	-	_	_	_
Critical Hdwy	6.42	6.22	_	_	4.12	-
Critical Hdwy Stg 1	5.42	-	_	_	-	_
Critical Hdwy Stg 2	5.42	_	_	_	_	_
Follow-up Hdwy	3.518	3.318	_	_	2.218	_
Pot Cap-1 Maneuver	973	1051			1570	
			-	-	15/0	-
Stage 1	998	-	-	-	-	-
Stage 2	1009	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver		1051	-	-	1570	-
Mov Cap-2 Maneuver	970	-	-	-	-	-
Stage 1	998	-	-	-	-	-
Stage 2	1006	-	-	-	-	-
J -						
Λ	\A/D		NE		0.0	
Approach	WB		NB		SB	
HCM Control Delay, s	8.7		0		3.2	
HCM LOS	Α					
Minor Lang/Major Myn	nt	NDT	NDDV	VBLn1	CDI	SBT
Minor Lane/Major Myn	IIL	NBT			SBL	
Capacity (veh/h)		-	-		1570	-
HCM Lane V/C Ratio		-	-	0.024		-
HCM Control Delay (s)	-	-	8.7	7.3	0
HCM Lane LOS		-	-	Α	Α	Α
HCM 95th %tile Q(veh	1)	-	-	0.1	0	-

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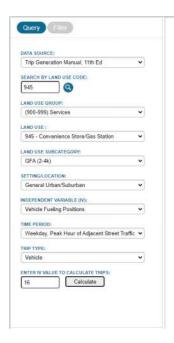
Drake Street TIA Approved Developments Trip Generation

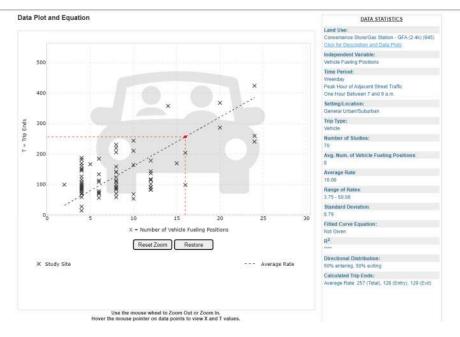
Convenier / Gas Stati								
		ADT	AM		AM	PM		PM
	VFP		Entering	Exiting	Volumes	Entering	Exiting	Volumes
Rate	16	3383	128	129	257	147	148	295
	Pass-by							
(76%AM/	75%PM)	i	97	98	195	110	111	221
Generate	ed Trips	1	31	31	62	37	37	74
40% In Network		-	13	13	26	15	15	30

Medical-Dental Office Building (720)											
		ADT	AM		AM	PM		PM			
	sqft		Entering	Exiting	Volumes	Entering	Exiting	Volumes			
Rate	62500	2096	136	32	168	44	134	178			
40% Ir	40% In Network		55	13	68	18	54	72			

Approved Development- Gas Station

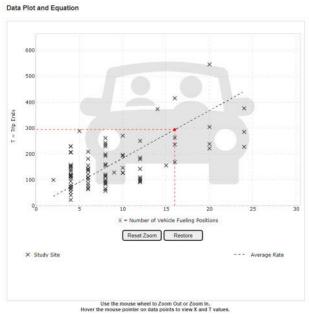
AM

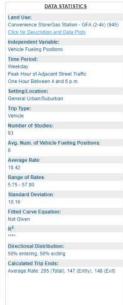




PM



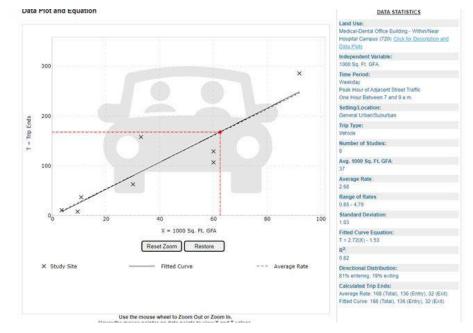




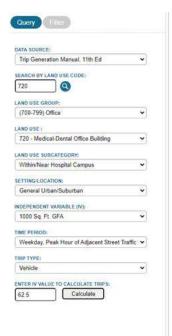
Approved Development- VA Expansion

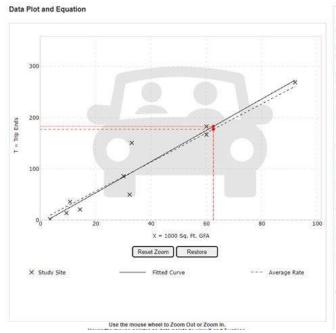
AM

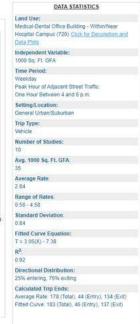




PM







Cliff Lawson

From: Chambers, Johnathan E < Johnathan.Chambers@columbiasc.gov>

Sent: Tuesday, September 6, 2022 10:35 AM

To: Cliff Lawson

Cc:Jeff Hochanadel; Burnette, Richard B (Brandon)Subject:RE: [EXTERNAL] Approved Development Question

Sounds good. Take care!

Johnathan



Johnathan E. Chambers, Land Development Administrator Planning and Development Services

1136 Washington Street, Columbia, SC 29201

Phone: 803.545.3206

johnathan.chambers@columbiasc.gov

www.columbiasc.gov/planning-development

From: Cliff Lawson < Cliff.Lawson@timmons.com>

Sent: Friday, September 2, 2022 8:36 AM

To: Chambers, Johnathan E < Johnathan. Chambers@columbiasc.gov>

Cc: Jeff Hochanadel < Jeff. Hochanadel@timmons.com>; Burnette, Richard B (Brandon)

<Richard.Burnette@columbiasc.gov>

Subject: RE: [EXTERNAL] Approved Development Question

Some people who received this message don't often get email from cliff.lawson@timmons.com. Learn why this is important

Hello Mr. Chambers,

From a site visit yesterday, I noted an Express Gas Station and the Fisher House project being constructed. I'll be sure to include those developments.

Thanks,

Cliff Lawson, PE, PTOE

Senior Project Manager

Office: 919.866.4946 | Fax: 704.376.1076

From: Cliff Lawson

Sent: Thursday, September 1, 2022 11:08 AM

To: Chambers, Johnathan E < <u>Johnathan.Chambers@columbiasc.gov</u>>

Cc: Jeff Hochanadel < Jeff. Hochanadel@timmons.com >; Burnette, Richard B (Brandon)

<Richard.Burnette@columbiasc.gov>

Subject: RE: [EXTERNAL] Approved Development Question

Hello Mr. Chambers,

In order to meet our project schedule, we are moving forward assuming there are no approved developments in the study area that will be built by 2023. If you have any questions, please let me know.

Thanks,

Cliff Lawson, PE, PTOE

Senior Project Manager

Office: 919.866.4946 | Fax: 704.376.1076

From: Cliff Lawson

Sent: Wednesday, August 24, 2022 10:22 AM

To: 'Chambers, Johnathan E' < Johnathan. Chambers@columbiasc.gov>

Cc: Jeff Hochanadel < Jeff. Hochanadel @timmons.com>; 'Burnette, Richard B (Brandon)'

<Richard.Burnette@columbiasc.gov>

Subject: RE: [EXTERNAL] Approved Development Question

Hello Mr. Chambers,

I just wanted to follow-up to see if there were any approved developments in the study area described in our previous email correspondence.

Thanks,

Cliff Lawson, PE, PTOE

Senior Project Manager

Office: 919.866.4946 | Fax: 704.376.1076

From: Cliff Lawson

Sent: Monday, August 15, 2022 11:30 AM

To: Chambers, Johnathan E < <u>Johnathan.Chambers@columbiasc.gov</u>>

Cc: Jeff Hochanadel < Jeff. Hochanadel@timmons.com>; Burnette, Richard B (Brandon)

<Richard.Burnette@columbiasc.gov>

Subject: RE: [EXTERNAL] Approved Development Question

This is a relatively small development so I would assume anything in a quarter mile.

Thanks,

Cliff Lawson, PE, PTOE

Senior Project Manager

Office: 919.866.4946 | Fax: 704.376.1076

From: Chambers, Johnathan E < Johnathan. Chambers@columbiasc.gov>

Sent: Monday, August 15, 2022 11:28 AM **To:** Cliff Lawson < Cliff.Lawson@timmons.com>

Cc: Jeff Hochanadel < Jeff. Hochanadel@timmons.com>; Burnette, Richard B (Brandon)

<Richard.Burnette@columbiasc.gov>

Subject: RE: [EXTERNAL] Approved Development Question

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Good morning! What proximity are you interested in?

Johnathan



Johnathan E. Chambers, Land Development Administrator Planning and Development Services

1136 Washington Street, Columbia, SC 29201

Phone: 803.545.3206

johnathan.chambers@columbiasc.gov

www.columbiasc.gov/planning-development

From: Cliff Lawson < Cliff.Lawson@timmons.com>

Sent: Thursday, August 11, 2022 5:10 PM

To: Chambers, Johnathan E < <u>Johnathan.Chambers@columbiasc.gov</u>>

Cc: Jeff Hochanadel < <u>Jeff.Hochanadel@timmons.com</u>> **Subject:** [EXTERNAL] Approved Development Question

You don't often get email from cliff.lawson@timmons.com. Learn why this is important

CAUTION: This email originated outside of the organization. Do not click links or open attachments from unknown senders or suspicious emails. Never enter a username or password on a site that you did not knowingly access.

Mr. Chambers,

My name is Cliff Lawson and I'm a traffic engineer with the Timmons Group. We have been contracted to complete a traffic impact analysis for a residential development off Drake Street (near Garners Ferry Road) in Columbia, SC (see image below). It is assumed this development will be built by 2023. I was given your contact information by David Brewer. Are you aware of any approved developments in the general area that will be built by 2023?

